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Geophysical Research Letters

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Supporting Information for

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Dynamic rupture process of the 2023 Mw 7.8 Kahramanmaras earthquake:

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Variable rupture speed and implications for seismic hazard

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Text S1, Figures S1 to S6 and Table S1.

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Additional Supporting Information (Files uploaded separately)

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Captions for Movies S1 to S2

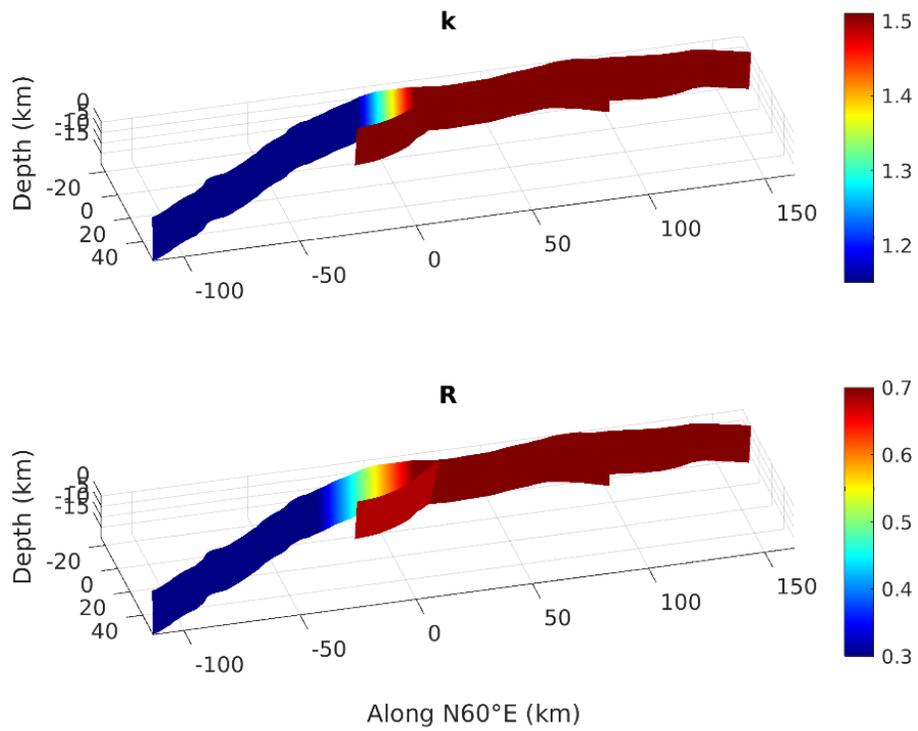
22 **Introduction**

23 This supporting material includes supplementary figures of stress and friction
24 parameter settings (Figure S1-S3), and a waveform comparison of several stations
25 with incomplete records (Figure S4). In addition, text S1 and Figure S5-S6
26 supplement the necessity of heterogeneous of the stress orientation and friction
27 coefficients.

28 **Text S1.** The necessity of heterogeneous of the stress orientation and friction
29 coefficients

30 We present the initial shear stress and relative fault strength S of three
31 homogeneous stress orientation case (Figure S5). It is obvious from the S value
32 that when the stress orientation is $N169^\circ$ or $N180^\circ$, the northeast segment of the
33 EAF will be very difficult to rupture (S value even smaller than 0, that is, the stress
34 drop is negative). Coincidentally, if the stress orientation is $N201^\circ$, the NPF and
35 the southwest segment of the EAF will be very difficult to rupture. Therefore,
36 consider the clockwise trend of stress orientation is necessary.

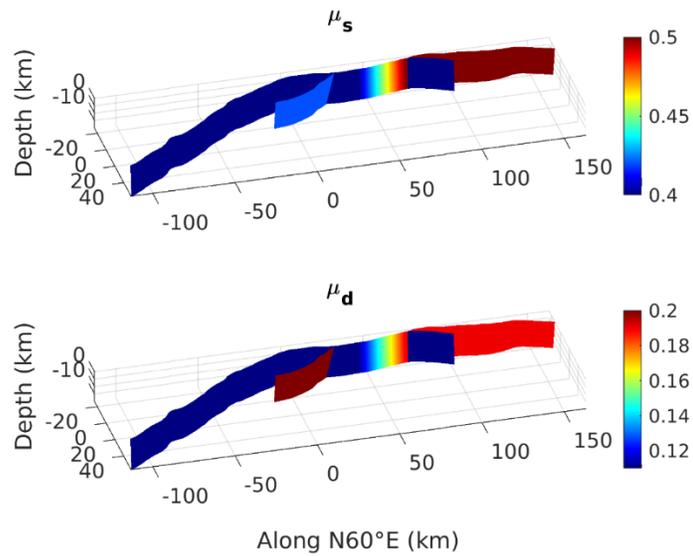
37 Furthermore, we calculate the distribution of initial shear stress and S value
38 when the friction coefficients of the EAF is uniform (Figure S6). From the S value,
39 we can expect that there will be a sustain supershear rupture in the northeast
40 segment of the EAF. However, in this case, the waveforms of the four stations in
41 Figure S4 will arrive earlier, and if so, these four stations should record more
42 waveforms before the recording stops suddenly. This is inconsistent with the
43 observation. Therefore, we increase the friction coefficients of the easternmost
44 segment of the EAF (see Figure S2) according to the geological survey results of
45 Khalifa et al. (2018).



46

47 Figure S1. The distribution of lateral pressure coefficient k and stress shape ratio
 48 R . On the NPF, $k = 1.51$ and $R = 0.68$. On the southwest segment of the EAF, $k =$
 49 1.15 and $R = 0.3$. On the F3 and the northeast segment of the EAF, $k = 1.51$ and
 50 $R = 0.7$.

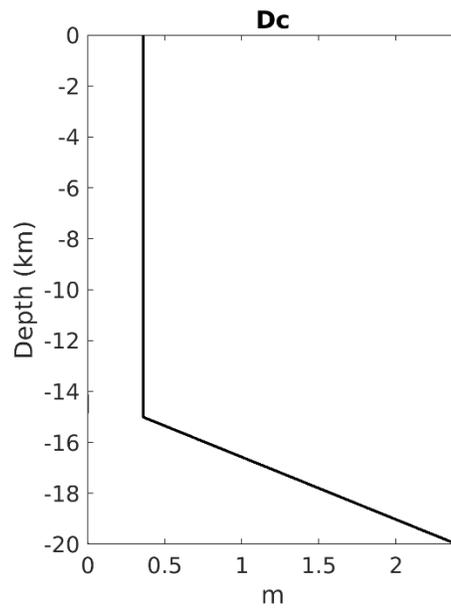
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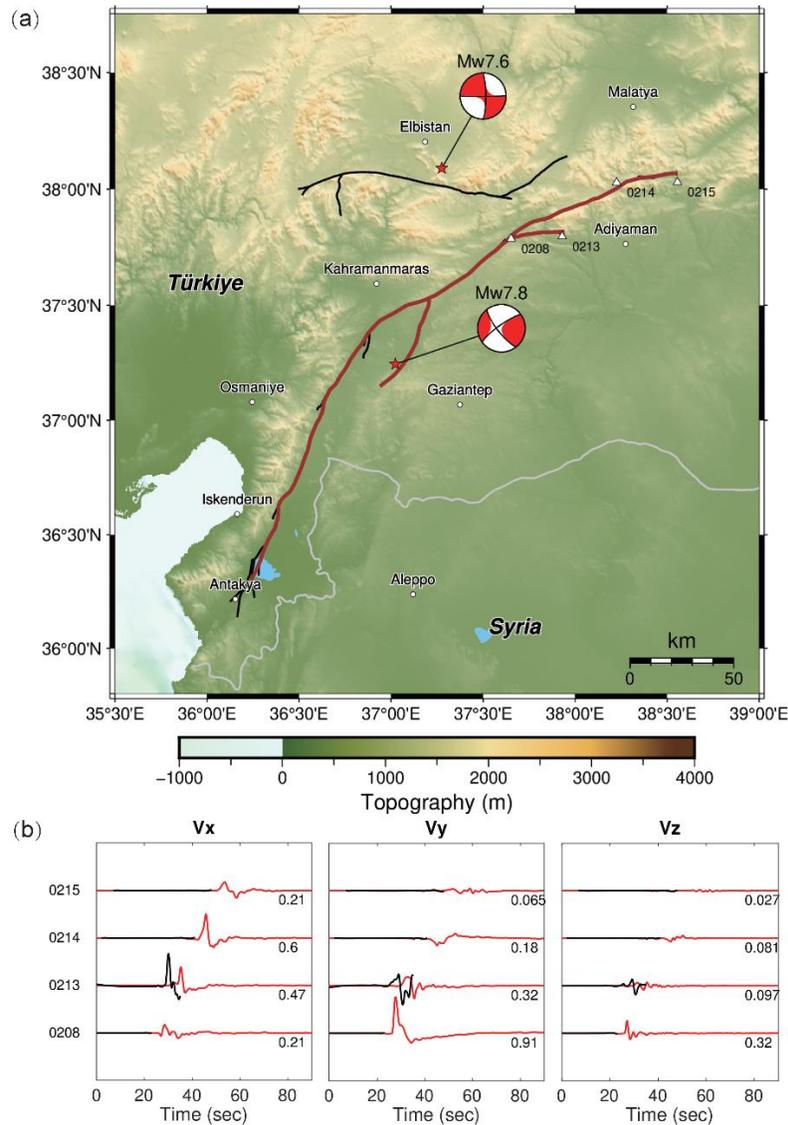
53 **Figure S2.** The distribution of static and dynamic friction coefficients μ_s and μ_d .
54 On the NPF, $\mu_s = 0.42$ and $\mu_d = 0.2$. On the F3 and the southwest segment of the
55 EAF, $\mu_s = 0.4$ and $\mu_d = 0.11$. On the northeast segment of the EAF, μ_s increases to
56 0.5 and μ_d increases to 0.19.

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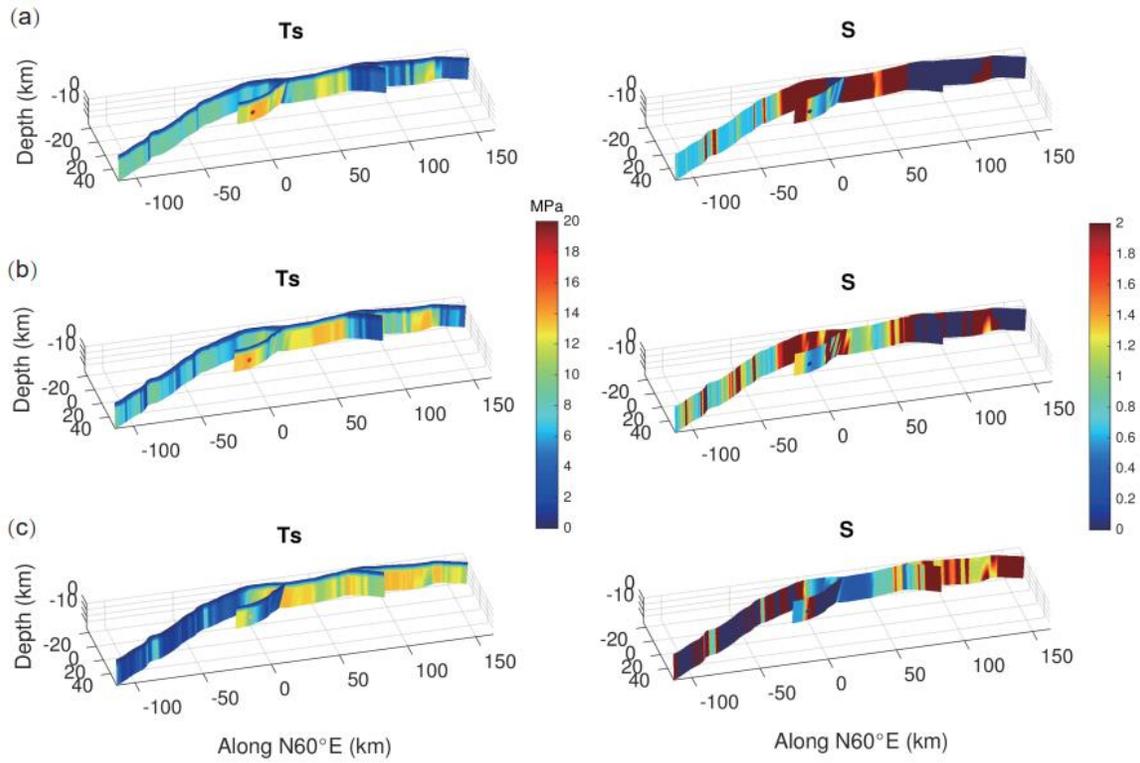
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59 **Figure S3.** Variation of critical slip distance D_c with depth. D_c reaches a
60 maximum of 2.4 m at a depth of 20 km.



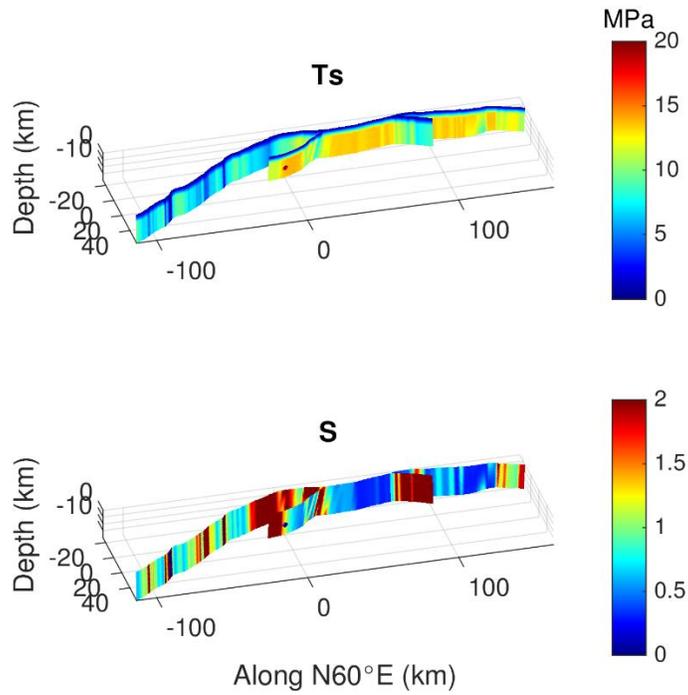
63 **Figure S4.** Comparison of incomplete waveform records of four near-fault
 64 stations in the northeast segment of EAF. (a) The location of four stations (white
 65 hollow triangle). Other things are same as Figure 1 in the text. (b) Waveform
 66 comparison. The black line is the observed waveform, and the red line is the
 67 synthesized waveform, both of which are filtered to 0.01-0.4 Hz. The station name
 68 is marked on the left. The maximum absolute values of each component of the
 69 synthesized waveform (m/s) are listed at the end of each seismogram.

70



71

72 **Figure S5.** Initial shear stress and relative fault strength S in different
73 homogeneous SH orientation cases. (a) SH orientation $N169^{\circ}E$; (b) SH orientation
74 $N180^{\circ}E$; (c) SH orientation $N201^{\circ}E$.



75

76 **Figure S6.** Initial shear stress and relative fault strength S with uniform friction

77 coefficient of the EAF.

78 **Tabel S1.** Layer velocity model used in the dynamic simulation (Form Güvercin et
79 al., 2022, Tabel S1)

Depth (km)	Vp(m/s)	Vs(m/s)
0	3880	2040
1	4520	2430
2	5620	3030
4	5750	3310
6	5850	3380
8	5960	3430
10	6000	3440
12	6050	3460
16	6320	3620
20	6400	3670
25	6830	3920
30	6890	3940
37	7800	4400
45	8220	4560
60	8300	4610

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81 **Movie S1.** Snapshots of slip rate from the dynamic rupture of the Mw 7.8
82 Kahramanmaras earthquake.

83 **Movie S2.** The ratio of shear stress and normal stress during the triggering
84 process. A ratio equal to μ_s (0.4) indicates the position of the rupture front in the
85 EAF.

86 **References in the Supporting Information**

87 Güvercin, S. E., Karabulut, H., Konca, A. Ö., Doğan, U., & Ergintav, S. (2022). Active
88 seismotectonics of the East Anatolian Fault, *Geophysical Journal*
89 *International*, 230(1), 50-69, <https://doi.org/10.1093/gji/ggac045>.

90 Khalifa, A., Çakır, Z., Owen, L., & Kaya, Ş. (2018). Morphotectonic analysis of the
91 East Anatolian Fault, Turkey, *Turkish Journal of Earth Sciences*, 27(2), 110-126,
92 <https://doi.org/10.3906/yer-1707-16>.

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