

1 Seismic discrimination of controlled explosions and earthquakes
2 near Mount St. Helens using P/S ratios

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10 **Key Points:**

11 1. Influences on local P/S ratios are analyzed with 23 shallowly buried explosions and 406 $M_L \geq 1$
12 earthquakes near Mount St. Helens.

13 2. Optimized array-median P/S ratios discriminate explosions with 100% true positives and
14 4.93% false positives.

15 3. P/S ratio variations at individual stations are interpreted as site effects that correlate with
16 shallow crustal velocity structure.

17

18 Abstract

19 Explosions and earthquakes are effectively discriminated by P/S amplitude ratios for moderate
20 magnitude events ($M \geq 4$) observed at regional to teleseismic distances (≥ 200 km). It is less clear
21 if P/S ratios are effective explosion discriminants for lower magnitudes observed at shorter
22 distances. We report new tests of P/S discrimination using a dense seismic array in a continental
23 volcanic arc setting near Mount St. Helens, with 23 single-fired borehole explosions (M_L 0.9-2.3)
24 and 406 earthquakes (M_L 1-3.3). The array provides up to 95 three-component broadband
25 seismographs and most source-receiver distances are < 120 km. Additional insight is provided by
26 $\sim 3,000$ vertical component geophone recordings of each explosion. Potential controls on local
27 distance P/S ratios are investigated, including: frequency range, distance, magnitude, source
28 depth, number of seismographs, and site effects. A frequency band of 10-18 Hz performs better
29 than lower or narrower bands because explosion-induced S-wave amplitudes diminish relative to
30 P for higher frequencies. Source depth and magnitude exhibited negligible influences. Site
31 responses for earthquakes and explosions are correlated with each other and with shallow crustal
32 V_p and V_s from travel-time tomography. Overall, the results indicate high potential for local
33 distance P/S discrimination in a continental volcanic arc setting, with 100% true positives and
34 4.93% false positives using a frequency band of 10-18 Hz for array-median P/S ratios.

35 Plain Language Summary

36 Methods to remotely classify seismic sources as either shear-slip earthquakes or shallow
37 subsurface explosions are important geophysical tools. They are used for investigations of
38 anthropogenic processes such as underground nuclear explosion tests and mining activity as well
39 as to obtain pure catalogs of tectonic and volcanic earthquakes. The ratio of compressional (P)
40 wave amplitude to shear (S) wave amplitude is effective for classifying large earthquakes and
41 explosions observed hundreds to thousands of kilometers away. Application of such methods at
42 local distances is a topic of growing interest because smaller magnitude sources are only
43 observed at close distances. We tested influences on P/S amplitude ratios and their effectiveness
44 for source discrimination using a data set of tectonic and volcanic earthquakes and controlled
45 shallow borehole explosions near Mount St. Helens. Most observations were within 120 km. We
46 found that use of high frequencies and array-median statistics is largely effective for source

47 discrimination in this setting, successfully classifying 100% of explosions while falsely
48 attributing about 5% of earthquakes to explosions. Variability of P/S ratios across the seismic
49 array has a highly similar pattern for explosions and earthquakes and that pattern appears to be
50 controlled by the seismic velocity structure of the shallow crust.

51 1. Introduction

52 Quantifying the distinctive properties of explosive seismic sources is an important capability for
53 identification and characterization of underground nuclear explosion tests and a key component
54 of verifying compliance with nuclear test-ban treaties (Bowers and Selby, 2009). Seismic
55 identification and characterization of explosions are also important in other contexts, such as
56 investigations of chemical explosions that may be the subjects of judicial investigations (e.g.,
57 Holzer et al., 1996; Koper et al., 2002, 2003) and volcanic explosions studied in the interest of
58 natural hazard mitigation (e.g., Neuberg et al., 1994; Rowe et al., 1998; Johnson and Lees, 2000).
59 Early research on seismic discrimination of nuclear explosions and earthquakes focused on
60 events that are observable at regional to teleseismic distances (≥ 200 km), which generally
61 requires $M \geq 4$ (Richards and Zavales, 1990). One useful seismic approach to discriminating
62 nuclear explosions and earthquakes at such distances is the measurement of P/S amplitude ratios.
63 Abundant empirical evidence confirms that large explosions ($M \geq 4$) produce greater P/S
64 amplitude ratios compared to tectonic earthquakes, although the observed ratios are regionally
65 heterogeneous (Taylor et al., 1989; Kim et al., 1993; Walter et al., 1995; Hartse et al., 1997; Xie
66 and Patton, 1999; Jenkins and Sereno, 2001).

67 Potential expansion of seismic discrimination techniques to local distances and lower
68 magnitudes (or explosive yields) has become a subject of increasing interest (Zeiler and Velasco,
69 2009; O'Rourke et al., 2016; Kolaj, 2018; Pyle and Walter, 2019; Holt et al., 2019; Kinter et al.,
70 2020). At local distances and lower magnitudes, methods are usually developed to discriminate
71 chemical explosions from earthquakes and, in some cases, to differentiate single-fired explosions
72 from delayed-fired explosions that are common in mining activity (Zeiler and Velasco, 2009;
73 O'Rourke et al., 2016). Single-fired chemical explosions in boreholes provide a useful proxy for
74 underground nuclear tests (Stump et al., 1999) and well-documented examples are available for
75 study on account of geophysical experiments targeting seismic source physics (e.g., Pyle and
76 Walter, 2019) or imaging of geological structures (e.g., O'Rourke et al., 2016). There is mixed
77 evidence regarding the effectiveness of P/S discrimination for $\leq M3$ events at distances of ≤ 200
78 km. Some empirical investigations report that failure to discriminate between earthquakes and
79 explosions may be restricted to the shortest distances (e.g., ≤ 50 km in O'Rourke et al., 2016).
80 Others report sporadic failures across the local distance range, potentially on account of
81 lithologic variability of the crust causing complex source and path effects that are more subdued

82 at regional to teleseismic distances (e.g., Pyle and Walter, 2019). Further research is needed to
83 address questions such as: Does the complexity of crustal wave propagation make P/S ratios less
84 diagnostic of explosive sources below a common distance threshold? Can diminished explosion
85 discrimination performance be overcome by larger seismic arrays or enhanced local calibration
86 using earthquakes to constrain site and/or path effects? What are the underlying differences in
87 explosion sources that control discrimination capability at local distances?

88 We use a data set with dense local distance recordings of earthquakes and single-fired
89 borehole explosions near Mount St. Helens to gain further insight into the seismic source and
90 structural properties that control the effectiveness of the P/S ratio explosion discriminant for low
91 yields (Fig. 1). Important aspects of the data set are its diverse source-receiver paths with most
92 distances <120 km and its combination of single-fired borehole explosions and earthquakes,
93 including shallow volcanic seismicity at Mount St. Helens (e.g., Ulberg et al., 2020; Glasgow et
94 al., 2018). The source-receiver distribution was optimized for 3D structural imaging, so the
95 source locations are not limited to one isolated test site or linear transect. The inclusion of
96 volcanic earthquakes near Mount St. Helens offers an interesting comparison because volcanoes
97 often produce more frequent shallow earthquakes and more variable source mechanisms
98 compared to other geologic settings.

99 2. Data

100 This study uses seismic recordings of earthquakes and single-fired chemical explosions in
101 shallow boreholes (Table S1). The explosions were detonated for the controlled source
102 component of the iMUSH project to image the magmatic system underlying Mount St. Helens
103 (Kiser et al., 2016, 2018; Hansen et al., 2016). Eight of the 23 boreholes were loaded with 907 kg
104 of explosive and the other 15 were loaded with 454 kg (Fig. 1b). The explosives were buried in
105 shallow boreholes with maximum depths of ~22-28 m and explosives occupying the bottom ~5
106 m of the boreholes. Earthquake source information from 2014 - 2016 was provided by the Pacific
107 Northwest Seismic Network, which contributes to the USGS Comprehensive Catalog (ComCat;
108 USGS, 2020). Earthquakes within 75 km of Mount St. Helens with $M_L \geq 1$ were considered for
109 the study. Lower magnitude earthquakes were not clearly recorded across most of the study area
110 so most seismograms would be removed by the requirement of signal-to-noise (SNR) >2.

111 Additionally, using $M_L \geq 1$ provides a close match to the magnitude range of the explosions (M_L
112 0.9-2.3).

113 The primary seismic waveform data for this study are from the broadband part of the
114 iMUSH project (Han et al., 2018; Crosbie et al., 2019; Mann et al., 2019; Ulberg et al., 2020),
115 which temporarily increased the density of local seismic monitoring. The iMUSH broadband
116 network (XD 2014-2016) was combined with permanent regional three-component broadband
117 stations to create a composite network of up to 95 stations within 75 km of Mount St. Helens
118 (Fig. 1a). Sampling rates vary among the networks. Based on the minimum sample rate of 40 Hz
119 we limited our analysis to frequencies ≤ 18 Hz. Network information for all the broadband data is
120 provided in Table S1. Examples of explosion and earthquake record sections from the broadband
121 array are shown in Figure 2. The example events have equal local magnitudes ($M_L=1.9$) and they
122 are plotted after application of bandpass filtering from 2-6 Hz. The explosion source exhibits a
123 stronger P-wave than the earthquake, while the earthquake exhibits a more prominent S-wave
124 than the explosion (Fig. 2).

125 A secondary source of seismic waveform data is vertical-component geophones deployed
126 during the iMUSH controlled source imaging experiment (Kiser et al., 2016, 2018; Hansen et al.,
127 2016). Our analysis of source discrimination using P/S energy focuses on three-component
128 recordings so we only present record sections from the vertical geophones to illustrate local
129 phase propagation (Fig. 3). In Figure 3, the geophone seismograms for all 23 explosions (70,944
130 source-receiver pairs) were sorted into 1 km distance bins and the median envelope in each
131 distance bin is plotted with trace-normalized amplitude. The high density of recordings illustrates
132 the existence of the S-wave starting at small distances and extending across the array.
133 Comparison of the 2-6 Hz envelopes in Figure 3a and 6-18 Hz envelopes in Figure 3b shows
134 diminished S-wave amplitudes relative to P for higher frequencies. Due to the short duration of
135 the geophone deployment and movement of most geophones during the experiment, there are
136 few opportunities for comparison with earthquakes that were recorded across most of the array.
137 Consequently, we focus on the broadband data from 2014 - 2016 for evaluation of P/S ratio as an
138 explosion versus earthquake discriminant.

139 3. Methods

140 3.1 P/S amplitude ratios

141 P/S ratios were measured with an approach similar to that used by O'Rourke et al. (2016). Below
142 we focus on the subtle differences with respect to use of three-component data and phase
143 windowing for amplitude measurements. O'Rourke et al. (2016) omitted the transverse
144 components for P measurements because a 1D isotropic medium should not produce P-wave
145 energy on the transverse component. In contrast to O'Rourke et al. (2016), we use all three
146 components for measurements of amplitude in P, S, and pre-event noise windows for both
147 earthquakes and explosions. P-wave energy is commonly observed on transverse components in
148 our dataset (Fig. 2), presumably due to out-of-plane scattering.

149 Phase windowing at local distances presents a challenge due to the decreasing separation
150 of P and S with decreasing distance. To maximize use of the data we scaled the window length
151 by the S-P time, so that the time window length increases with distance until reaching a fixed
152 duration. The time window starts at -5% of the S-P time before the phase arrival time (P, S or
153 Noise) and ends at 50% of the S-P time after the arrival time for shorter source-receiver
154 distances. At larger distances (i.e., beyond 40 km) a fixed value of 3 sec after the arrival time
155 (Fig. 4) is used for the end of the measurement window. Stations that are too close to an event
156 (i.e., produce a S-P time window less than 1 sec) are discarded because they prevent reliable
157 separation of P and S amplitudes and their arrival times are more variable. Pre-event noise time
158 windows were sampled starting at 10 sec before the origin time of each explosion or earthquake
159 source. Our goal is to ensure the maximum phase energy is captured within the windows while
160 minimizing the contamination from noise or interfering phases. Although the optimization of
161 phase-windowing is somewhat arbitrary, consistent P/S ratio results were achieved in additional
162 tests with the maximum window length increased to 4, 5, and 6 sec. We focus on the 3 sec
163 window results for the remainder of the text.

164 The phase windows shown in Figure 4 were calculated using a local 1D P and S velocity
165 model derived from the controlled source survey (Fig. 1b and Fig. S1; Kiser et al., 2016). Events
166 with P-wave root-mean-square amplitude $SNR > 2$ were retained for P/S ratio measurements (Fig.
167 S2). Stability in the results for different phase window lengths from 3-6 sec indicates that the

168 deviations from the predicted 1D arrival times have little effect. This is not surprising because
169 phase picks for the explosion sources from Ulberg et al., (2020) have small travel time residuals
170 compared to the 3 sec window length (Fig. 4). Residual times for 1309 manually picked P phases
171 from explosions recorded by the broadband array have a standard deviation of 0.3 sec (average
172 0.01 sec), much smaller than our window width. Manual picks are unavailable for many P and S
173 phases at individual stations because only the clearest arrivals are picked. Thus, we prefer the
174 generic phase windowing approach using the 1D velocity model and 3 sec phase windows for
175 consistency and to avoid biasing amplitude measurements by under-representing weak S-waves
176 that are important to source discrimination.

177 After phase windowing the three-component P/S ratio (R) at a given station (n) was
178 calculated as:

$$179 \quad R_n = \frac{\sqrt{P_i^2 - N_i^2}}{\sqrt{S_i^2 - N_i^2}}, \text{ Eq(1)}$$

180 where the subscript i denotes summation of the three seismogram components. For source
181 discrimination tests, the array median and scaled median absolute deviation (SMAD) of all the
182 individual P/S ratios are used. P/S ratios were measured with waveforms bandpass filtered in
183 several frequency bands. We tested narrow frequency bands of 2-4 Hz, 4-6 Hz, 6-8 Hz, 8-10 Hz,
184 10-12 Hz, 12-14 Hz, and 14-16 Hz, following O'Rourke et al., (2016). We also tested two
185 broader frequency bands of 6-12 Hz and 10-18 Hz. In each case a two-pole Butterworth filter
186 was applied to the response-corrected waveforms after demeaning and detrending.

187 **3.2 Bootstrap resampling for different array sizes**

188 The temporary broadband array (XD), in combination with the permanent networks (UW, CC),
189 provides better seismic sampling than is available for many areas of interest for explosion
190 monitoring (Fig. 1a). Although up to 95 stations are available during the 2-year period, not all
191 stations/components are available the entire time and meet the $\text{SNR} > 2$ threshold. Within our
192 preferred frequency range (10-18Hz), the number of stations that are finally used for P/S ratio
193 calculation for explosions ranges from 36 to 78, with an average of 66. The average number of
194 stations for $M_L \geq 2$ and $M_L 1-2$ earthquakes are 72 and 47, respectively. To fully evaluate the
195 potential of our preferred method and parameter set, we used bootstrap resampling test to

196 simulate results for six subset array sizes: 2, 4, 8, 16, 32, and 64. For each subset, the cumulative
197 array was randomly resampled 1,000 times (without replacement) from the 74 common stations
198 that recorded all earthquakes and explosions without any prerequisite (i.e., SNR). Within each
199 sampled set, the array-median P/S ratio for earthquakes and explosions are calculated after
200 applying the SNR control. In the other words, the bootstrapping approach attempts to simulate
201 scenarios with smaller arrays and an unconditioned distribution of SNR recordings.

202 **3.3 Site corrections for P/S ratios**

203 We estimated station-based site corrections using P/S ratios of earthquakes. This was chosen to
204 mimic the circumstance in which P/S corrections could be estimated using only earthquake data
205 and then applied to subsequent events of unknown physical origin. The correction is calculated
206 as a normalization of event-averaged P/S ratio at each of the N stations:

$$207 \quad C_{1,2,3\dots N} = R_{eq@station(1,2,3\dots n)} / \text{mean}(R_{eq@station(1,2,3\dots n)}), \quad \text{Eq}(2)$$

208 Where, $R_{eq@station(1,2,3\dots n)}$ is a vector that contains N values, each corresponding to an event-
209 averaged P/S ratio (i.e., calculated from up to 406 earthquakes) at a given station after the SNR
210 control. For each event (explosion or earthquake) recorded at a subset of m stations, its P/S ratio
211 is then corrected by dividing $C_{1,2,3\dots m}$. The outcome of site correction is discussed in section 4.5
212 and R_{eq} for the entire array is presented in Figure 9b.

213 **4. Results**

214 **4.1 Optimal frequency content**

215 Array median P/S ratios for explosions are greater than for earthquakes in all frequency bands
216 (Fig. 5). However, the one SMAD intervals of P/S ratios overlap for lower frequency bands and
217 most narrow frequency bands. Distributions of P/S ratios are typically not Gaussian (i.e., long-
218 tailed), so the SMAD is preferred instead of the standard deviation. In general, higher bands
219 provide larger separation in the median P/S ratios between earthquakes and explosions, while
220 broader bands help to decrease the variance and stabilize discrimination of individual events
221 (Fig. 5). With respect to source discrimination, 10-18 Hz is the preferred frequency band for this
222 local distance data set. The 14-16 Hz band also performs well but for individual events it is more

223 variable and may reduce the number of $\text{SNR} > 2$ phase windows for analysis. The 10-18 Hz array-
224 median P/S ratios and SMAD values for earthquakes and explosions are $1.72(\pm 0.34)$ and
225 $0.46(\pm 0.19)$, respectively. P/S ratios for both earthquakes and explosions increase with
226 frequency, however the increase with frequency is greater for the explosions (Fig. 5). This result
227 from analysis of the three-component broadband array data is consistent with the observation
228 from the vertical-component geophones showing that S-wave amplitude diminishes relative to P
229 for higher frequencies (Fig. 3).

230 **4.2 Distance, magnitude, and depth effects**

231 We focus on results from distances < 120 km because most of the available source-receiver pairs
232 are within that distance range (Fig. 4b). Median P/S ratios for earthquakes and explosions sorted
233 into six 20 km wide distance bins show little change at shorter distances and then increasing P/S
234 ratio with distance beyond ~ 60 km (Fig. 6a). The SMAD values are also larger at greater
235 distances due to the decreased number of samples within each distance bin. Given that distance
236 distributions of earthquakes and explosions are very similar in this study (Fig. 4b), we do not
237 apply distance corrections to the P/S ratios.

238 P/S ratios for earthquakes and explosions do not vary strongly with local magnitude (Fig.
239 5b). The median P/S ratios in most $0.2 M_L$ bins overlap within one SMAD. There appears to be
240 an increase in P/S ratio for the largest explosion magnitude bin, but it is heavily influenced by
241 one explosion source with a particularly high P/S ratio resulting in a relatively large SMAD for
242 the highest magnitude bin among explosions (Fig. 5b). Earthquake P/S ratios remain low across
243 the local magnitude range. There is a slight decrease in the median earthquake P/S ratios for the
244 largest magnitudes ($M_L > 2.5$), which is within the range of one SMAD. Given the weak distance
245 and magnitude dependences found in the P/S ratios, we did not apply the magnitude and distance
246 amplitude correction (MDAC) approach that is commonly used in regional distance studies
247 (Anderson et al., 2009).

248 Estimated earthquake source depths also do not exhibit a clear correlation with P/S ratios
249 (Fig. 7). As the area near Mount St. Helens is characterized by variable surface topography (i.e.,
250 ranging from 0 - 4 km, Fig. 1), we also take the topography into account and calculate the
251 relative distance to the surface (instead of absolute depth to sea level). Binning the earthquake
252 sources into four depth ranges (0-5, 5-10, 10-15, and 15-20 km) results in median P/S ratios that

253 all overlap with one SMAD. Depth uncertainties are highly variable depending on local array
254 coverage, but reported uncertainties from the Pacific Northwest Seismic Network for $M_L \geq 1$
255 earthquakes near Mount St. Helens are typically < 1 km. In that context, results from binning
256 within 5-km depth intervals should not be strongly biased by inaccurate depth estimates. There is
257 a slight decrease in median P/S ratio from 0.3 at 0-5 km to 0.26 at 15-20 km, which is within the
258 SMAD (i.e., 0.07-0.14) for any of the source depth bins.

259 **4.3 Number of stations in the seismic array**

260 Bootstrap resampling of the three-component seismographs simulates the potential average
261 source discrimination performance with smaller seismic arrays (see section 3.2). The cumulative
262 distribution functions (CDFs) from resampling show that greater variations are observed for
263 explosion P/S ratios compared to earthquake P/S ratios (Fig. 8). Increasingly large seismic arrays
264 help reduce the overlap of earthquake and explosion P/S ratio distributions near a value of ~ 1
265 (Fig. 8). Separation of earthquake and explosion P/S ratios is subject to diminishing
266 improvement for arrays with over 16 stations. The improvement with increasing array size
267 appears modest in this context because the curves shown in Figure 8 are generated as averages
268 from 1,000 bootstrap resampling subsets (for 2, 4, 8, 16, 32 and 64 station cases). The variance
269 of P/S ratios is much larger for smaller arrays and its effect on discrimination performance is
270 discussed further in section 5.1.

271 **4.4 Site response effects and shallow crust structure**

272 Variations in station-averaged P/S ratios from earthquakes and borehole explosions exhibit
273 similar spatial patterns, despite the generally higher P/S ratios for explosions (Fig. 9). A scatter
274 plot of the earthquake station-averages versus the explosion station-averages shows an
275 approximately linear trend, with a correlation coefficient of 0.625. If the earthquakes are subset
276 by magnitude, the $M_L 1-2$ and $M_L \geq 2$ subsets yield correlations of 0.625 and 0.641 (these two
277 earthquake subsets are correlated at 0.91), respectively. These correlations indicate that
278 observations of small ($\sim M_L 1-3$) earthquakes may provide a useful basis for determining
279 empirical P/S amplitude site corrections that are applicable to explosions. However, the
280 improvement for the purpose of source discrimination appears to be subtle in this case (Fig. 10).

281 Application of site corrections increased the difference between the median explosion and
282 earthquake P/S ratios from 1.29 to 1.41, but the SMAD values also increased slightly for
283 explosions (0.38 to 0.43) and earthquakes (0.21 to 0.23). Furthermore, we found the site
284 correction terms are positively correlated with shallow crustal velocities. We adopted a velocity
285 model from a recent local travel time tomography study around Mount St. Helens (Ulberg et al.,
286 2020) and compared our site corrections with the V_p , V_s and V_p/V_s values beneath all the
287 station (site) locations. At 1km depth, the cross-correlation coefficients for the site correction
288 terms are 0.397 for V_p and 0.479 for V_s . Site corrections exhibit a much weaker correlation of -
289 0.086 with V_p/V_s (Fig. 9 d-f). The correlation coefficients remain comparable for all layers
290 around sea level (± 2 km) and they decrease at deeper depths, suggesting that the site correction is
291 influenced by uppermost crustal structure.

292 5. Discussion

293 5.1 Effectiveness for explosion discrimination

294 Receiver operating characteristic (ROC) curves show the diagnostic performance of binary
295 classifiers, in this case for explosions versus earthquakes, using a variety of discrimination
296 thresholds (Fig. 11). For each P/S ratio used as a discrimination threshold the point along the
297 ROC curve is determined by the rate of true positives and false positives. The optimal
298 discrimination threshold is chosen by maximizing the area under the curve (AUC), thus an ideal
299 classifier would plot in the upper left corner corresponding to 100% true positive and 0% false
300 positives. Application to P/S ratios with the preferred frequency band of 10-18 Hz and the full
301 data set of earthquakes and explosions shows 100% true positives and 4.93% (20 out of 406)
302 false positives for a P/S ratio threshold of 1.2 (Fig. 11a). Half of the events that create false
303 positives (i.e., $P/S > 1.2$) are only recorded with < 6 stations, reflecting the disadvantage of
304 insufficient station coverage for low-magnitude sources (Fig. S3). For comparison, a lower and
305 narrower frequency band of 6-8 Hz results in 86.95% true positives and 5.67% false positives for
306 a P/S ratio threshold of 0.9.

307 Discrimination performance generally improves with increasing event magnitude and
308 array size (Fig. 11c, d). Using all explosions and only $M_L \geq 2$ earthquakes, a threshold P/S ratio of
309 1.2 results in 100% true positives and 0% false positives. The M_L 0.9-2.3 explosions produced an

310 average of 66 stations with $SNR > 2$, while the M_L 1-2 earthquakes only produced an average of
311 47 stations with $SNR > 2$. So, the diminished discrimination performance for M_L 1-2 earthquakes
312 is likely influenced by SNR at individual stations and the total number of stations available for
313 analysis. ROC curves for seismic arrays composed of $N=4$, 16, and 64 seismographs illustrate
314 the effects of array size (Fig. 11c). For $N=64$, the bootstrap resampling results show that a
315 maximum AUC of 1 is consistently achieved for discrimination of explosions and $M_L \geq 2$
316 earthquakes. For $N=16$, the average of the AUC maxima is 0.98. For $N=4$, the average of the
317 AUC maxima reduces to 0.94 (Fig. 11d). However, the ROC curves for $N=4$ are much more
318 variable, including a few samples with near-random performance (Fig. 11c) and some extreme
319 cases reaching the AUC maximum (Fig. 11d). Generally, larger array size is expected to better
320 mitigate source/path variations. A separate bootstrap resampling test with an earthquake
321 epicenter nearly co-located with an explosion shows that < 16 stations are sufficient for robust
322 discrimination (Fig. S4), suggesting that minimum number of stations could be much lower if the
323 earthquake and suspected explosion are closely located with depth difference (i.e., as an ideally
324 case). In this example the horizontal locations are separated by 2.4 km and the depths are
325 separated by 11.1 km.

326 Comparison of the new results from near Mount St. Helens with other local distance P/S
327 ratio discrimination tests may be influenced by different local propagation effects related to
328 geological settings as well as measurement approaches. A similar scale study using data covering
329 the Bighorn mountain range and adjacent sedimentary basins in Wyoming found effective P/S
330 discrimination at ~ 50 -200 km distance but failure at < 50 km distance (O'Rourke et al., 2016).
331 Below we consider two minor methodological differences between this study and O'Rourke et
332 al. (2016) that might contribute to the difference in performance. We acknowledge that different
333 local propagation effects may also be the cause of the difference, but a thorough re-analysis of
334 their data would be required to isolate that influence.

335 The first methodological difference is that we include the transverse component for P-
336 wave measurements (see section 3.1). Explosion recordings in this study commonly show
337 $SNR > 2$ (our threshold for analysis) even for P-waves recorded on the transverse component (Fig.
338 2). If scattering of P energy onto the transverse component is important at distances < 50 km, then
339 the inclusion of transverse component data may be beneficial for explosion discrimination. A
340 comparison of array-median P/S ratios with and without the transverse component shows that

341 separation of the explosion and earthquake ratios improves with inclusion of the transverse
342 component (Fig. 12). The increased separation is primarily due to increases in the explosion P/S
343 ratios, while changes in the earthquake P/S ratios are smaller. This is consistent with the
344 possibility that out-of-plane P-wave scattering is stronger for explosions than earthquakes. In this
345 case, the benefit of including transverse component P-wave energy spans our entire local
346 distance range (Fig. 12), but given that P/S ratios tend to increase with distance for both
347 approaches the incremental improvement is more important at smaller distances (≤ 60 km).

348 The second difference is that we did not apply the MDAC method for regional seismic
349 discriminants (Anderson et al., 2009) to correct for distance and magnitude effects. We chose not
350 to use MDAC because the distance and especially magnitude trends in our raw P/S ratios are
351 modest compared to the SMAD values for explosion and earthquakes, respectively (Fig. 6).
352 Additionally, O'Rourke et al. (2016) note that stations at their shortest distances (~ 20 -40 km)
353 exhibit abnormally high MDAC corrections for explosions. We speculate that the amplitude
354 correction techniques developed for regional distances may need to be revised for shorter local
355 distances. Similar to the weak distance and magnitude trends found in this study, Zeiler and
356 Velasco (2009) reported negligible distance dependence of explosion discriminants (including
357 P/S ratios) within the local distance range. We suggest that the necessity and design of the
358 amplitude correction techniques for explosions observed at short distances (≤ 50 km) should be
359 further investigated.

360 In a recent local to regional distance study, Pyle and Walter (2019) investigated P/S ratio
361 discrimination with six chemical explosions from the Source Physics Experiment (Snelson et al.,
362 2013) and nearby tectonic earthquakes. Similar to O'Rourke et al. (2016) and this study, Pyle
363 and Walter (2019) found that P/S discrimination performance improved with increasing
364 frequency (≥ 6 Hz) and that array averaging of ~ 10 or more stations was needed to achieve clear
365 separation of explosion and earthquake P/S ratios. Four of the six explosions used in their study
366 had larger explosive yields than all the explosions in this study and the receiver spacing within
367 ~ 100 km was sparser, so relative to O'Rourke et al., (2016) there is less opportunity for
368 comparison of results at similar scales. The fact that we observe optimal performance for
369 somewhat higher frequencies in this study (e.g., 10-18 Hz) likely reflects our focus on shorter
370 source-receiver distances of < 120 km compared to distances up to ~ 450 km in Pyle and Walter,
371 (2019).

372 **5.2 Source effects**

373 The geophone record sections show that S-waves emerge within the first few kilometers from the
374 source, acknowledging that there is not sufficient sampling available to resolve S-wave
375 emergence in detail at scales of hundreds of meters (or less) from the source (Fig. 3). Assuming
376 the S-wave is effectively generated at the source for this data set, increasing P/S ratio with
377 distance is expected if S-wave attenuation is greater than P-wave attenuation in the crust (e.g.,
378 Pyle et al., 2017). In contrast, a difference in source spectra may be needed to explain why
379 explosion P/S ratios increase with frequency more than earthquake P/S ratios (Fig. 5).

380 Prior studies of $M \geq 3$ chemical explosions and nuclear explosions indicate that explosion-
381 induced crustal S-waves (Lg) exhibit lower corner frequencies than explosion-induced P-waves
382 (local Pg & regional Pn phases; Xie, 2002; Fisk, 2006, 2007). In these studies, the S-wave corner
383 frequency is typically about half of the P-wave corner frequency. Our results with lower yield
384 chemical explosions are similar based on the increased separation of local distance explosion and
385 earthquake P/S ratios at higher frequencies. The 10-18 Hz band may perform relatively well for
386 P/S ratio discrimination because it partially overlaps the interval between the lower S-wave
387 corner frequency and the higher P-wave corner frequency (e.g., Fisk, 2007). Using the Mueller-
388 Murphy model corner frequency scaling from Fisk, (2007) the explosions in this study are
389 expected to produce local P-wave corner frequencies of ~35-45 Hz and S-wave corner
390 frequencies of ~17-23 Hz (Fig. S5). The 40 Hz sampling rate for most stations limited our
391 analysis to frequencies below ~18 Hz, so only the highest frequencies in this study are near the
392 expected S-wave corner. Extension of P/S ratio measurements to higher frequencies by
393 collecting higher sample-rate data may be beneficial, especially for very short distances (≤ 50
394 km) and low magnitudes ($M_L \leq 2$).

395 The physical controls on explosion-induced S-wave spectra remain debated. If a
396 difference in source spectra explains the observed frequency dependence of P/S ratios, the
397 physical cause may be rooted in the different P and S elastic length scales of sensitivity to near-
398 source rock damage (Taylor, 2009). However, a variety of complicated and locally specific
399 effects such as spall and free-surface topographic scattering are thought to influence explosion-
400 induced S-wave spectra so there may not be one dominant explanation (e.g., Xie and Lay, 1994;
401 Patton and Taylor, 1995). An alternative to explaining the frequency dependence of P/S ratios

402 with different source spectra is that explosions may preferentially excite shallower shear modes
403 that attenuate more rapidly with distance (e.g., Baker et al., 2004, 2012).

404 One explosion source in this study that produced a relatively low P/S ratio resulted in
405 clear surface evidence of shear slip at the source. The ‘X4’ explosion (Fig. 1b; also see Table S1)
406 detonated in a borehole with maximum depth of ~22 m depth resulted in a small normal fault
407 scarp with a length of ~15 m and vertical offset of up to ~20 cm. Consequently, it is unsurprising
408 that this explosion exhibited a relatively low P/S ratio of 1.27 (Fig. 10), which is near the optimal
409 binary classification cutoff of 1.2 for 10-18 Hz the data set including all $M_L \geq 1$ earthquakes (Fig.
410 11b). It is unknown if ‘blind’ shear failures that did not rupture the surface are common for other
411 low P/S ratio explosions.

412 **5.3 Combining local distance seismic discriminants**

413 Ratios of different seismic magnitude metrics such as m_b & M_s have long been used as an initial
414 or ‘screening’ step for source discrimination of $M \geq 3$ events (Stevens and Day, 1985; Selby et
415 al., 2012; Ford and Walter, 2014). At local scales there is growing evidence that the difference
416 between the local (Richter) magnitude and the coda duration magnitude ($M_L - M_C$) can help
417 discriminate explosions, primarily because the magnitude difference is sensitive to source depth
418 (Holt et al., 2019; Voyles et al., 2020). Very shallow sources such as borehole explosions
419 preferentially produce longer coda leading to negative $M_L - M_C$. P/S amplitude ratios ignore the
420 extended coda and we find negligible depth dependence for P/S amplitude ratios in this study
421 (Fig. 7). Thus, the capabilities of the two discriminants appear to be rooted in complementary
422 aspects of the local seismic wavefield. A simple workflow to leverage the two approaches would
423 be using $M_L - M_C$ to screen for unusual events given that routine catalog generation can commonly
424 provide both parameters. Then events identified by screening could be further investigated with
425 P/S ratios. More thorough approaches to jointly classifying events based on $M_L - M_C$ and P/S
426 ratios should also be considered. P/S ratio measurements could also be automated to enhance
427 screening capabilities once travel time relationships and site corrections are developed for an
428 array. Additional use of more time-consuming moment tensor analysis of low magnitude local
429 distance events might be reserved for events flagged by $M_L - M_C$ and P/S screening (e.g., Alvizuri
430 and Tape, 2016).

431 6. Conclusions

432 P/S ratio discrimination of earthquakes and shallow single-fired borehole explosions at distances
433 less than 120 km was tested with a dense broadband seismic array near Mount St. Helens. Taking
434 advantage of the excellent coverage of both stations and sources, we evaluated the effects of
435 frequency bands, source-receiver distances, source magnitudes and focal depths. Optimal
436 separation of P/S ratios for the two sources types was found using a 10-18 Hz frequency band,
437 which achieved explosion discrimination with 100% true positives and 4.93% false positives
438 using the entire array. Randomly resampling to simulate smaller arrays shows performance of
439 $\geq 98\%$ true positives and $\leq 6.3\%$ false positives for ≥ 16 stations. Performance becomes highly
440 variable using ≤ 4 stations. Successful separation using the dense array and optimized frequency
441 band left limited room to improve the performance, consequently our site corrections derived
442 from 406 local earthquakes had a negligible effect on discrimination statistics. Despite the
443 limited improvements in this case, we found that the site corrections correlate with V_p and V_s of
444 the uppermost crust from a recent tomography study. Future studies using P/S ratios may benefit
445 from local site corrections derived from small earthquake recordings or local tomography
446 models.

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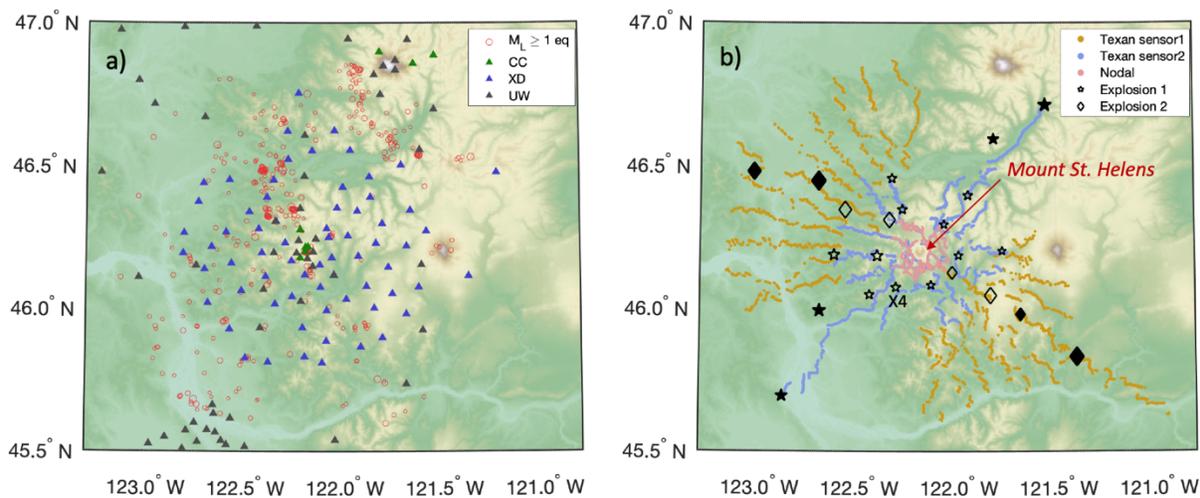
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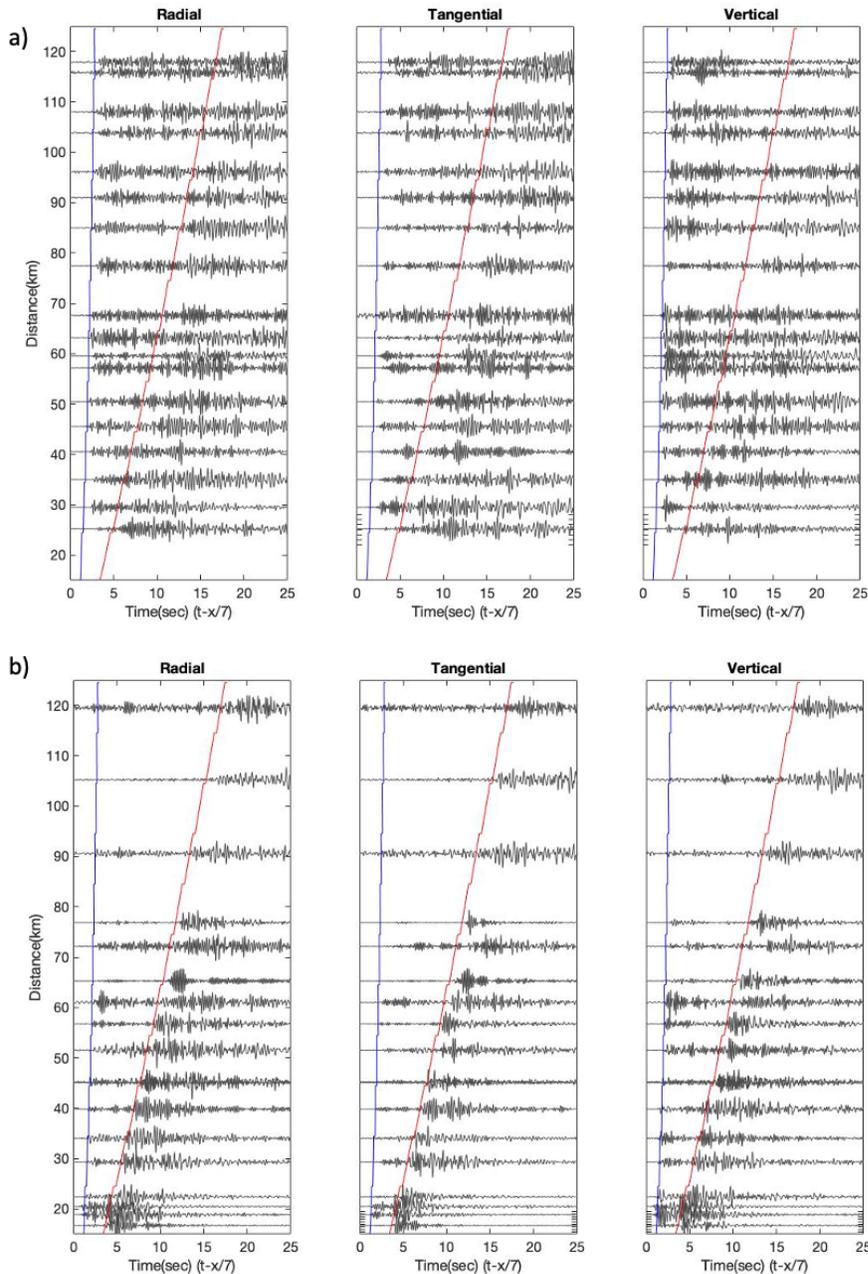
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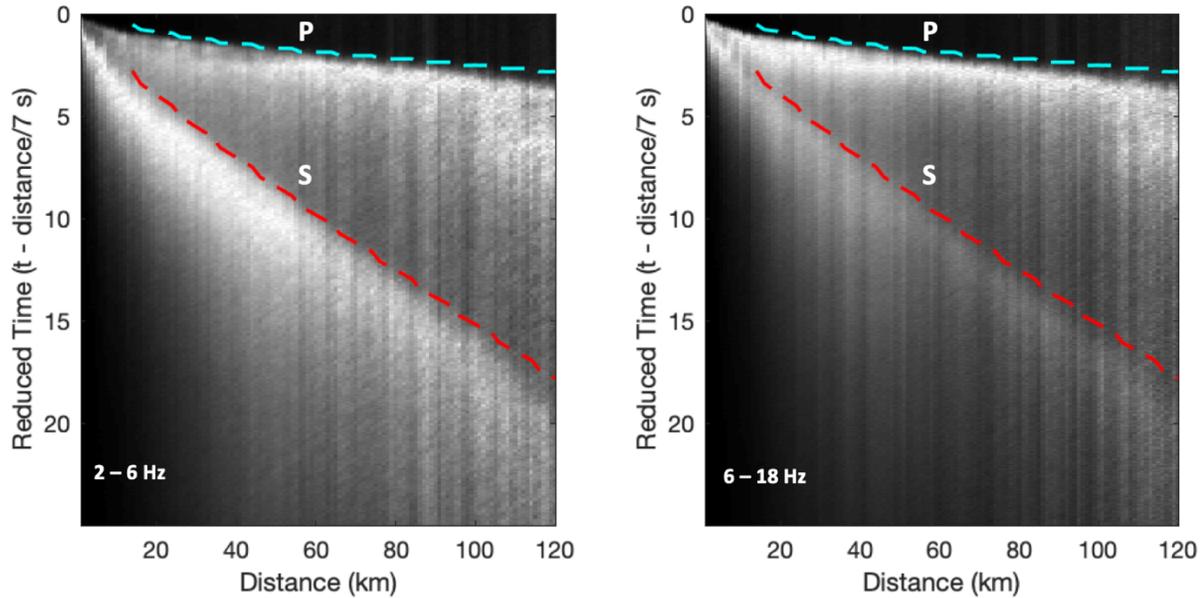


581
 582 Figure 1. Study area maps with sources and receivers. A) Broadband stations used in the study
 583 are plotted along with the locations of $M_L \geq 1$ earthquakes that occurred between June 20, 2014 to
 584 August 31, 2018 (i.e., time span for XD array) within 75 km of Mount St. Helens. B) Vertical
 585 geophone locations are plotted along with single-fired explosion locations. Explosion locations
 586 loaded with 907 kg of explosive are denoted by filled symbols and locations loaded with 454 kg
 587 are denoted by hollow symbols. The symbol sizes for explosions are scaled by their M_L .
 588 Explosions labeled with stars were detonated during controlled source phase 1 (recorded by
 589 Texan 1 array; ~2370 nodes) and diamonds were detonated during phase 2 (recorded by Texan 2
 590 array; ~2220 nodes). ‘X4’ denotes one explosion that is discussed in the text. Geophone
 591 locations in pink (~900 nodes) recorded both sets of explosions.



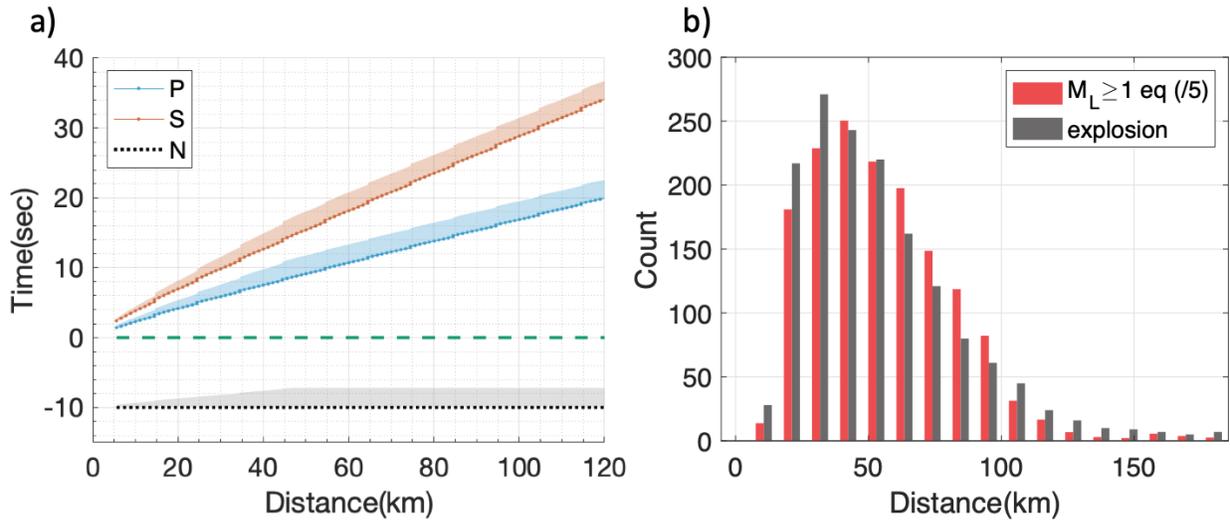
592

593 Figure 2. A) A record section is plotted for an explosion event with 616kg equivalent TNT load
 594 (Y8, located at the NW of array, $M_L=1.9$; see Table S1 for details). The event showed relatively
 595 strong S energy among explosions. Only 18 seismograms are shown for clarity. B) Record
 596 section for an equal-magnitude earthquake (2015 Feb 9, 05:45:35) with waveforms from 19
 597 stations. Waveforms are filtered between 2-6 Hz at plotted with a reduced velocity of 7 km/s in
 598 both figures. The blue and red lines mark the predicted P and S wave arrivals, respectively, using
 599 a locally optimized 1D velocity model (Kiser et al., 2016; also see Fig. S1).



600
 601 Figure 3. Stacked geophone recordings of explosions. A) Median envelopes of geophone
 602 seismograms from all 23 explosions in 1 km distance bins (70,944 source-receiver pairs).
 603 Seismograms were bandpass filtered from 2-6 Hz before envelope calculation and median-
 604 stacking. Median envelopes at each distance are normalized by their maximum. The cyan dashed
 605 line marks the beginning of the P window and the red dashed line marks the beginning of the S
 606 window. B) Same as A, except that seismograms were bandpass filtered from 6-18 Hz. The
 607 higher frequency band exhibits diminished S-wave amplitudes relative to P.
 608

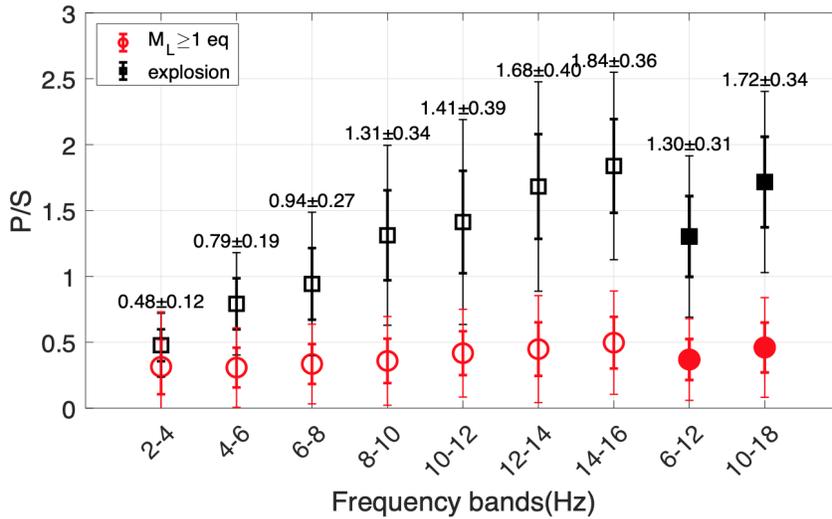
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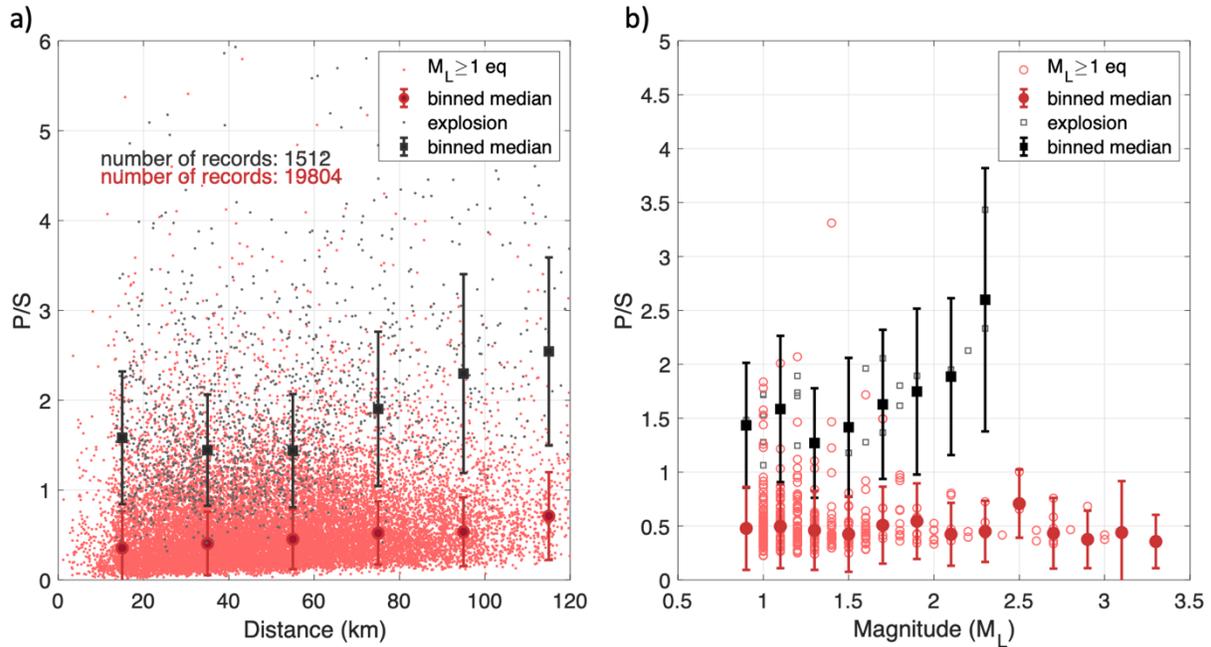
611 Figure 4. Phase windowing and source-receiver distances. A) Phase windowing based on travel
 612 times from a local 1D P and S velocity model (Kiser et al., 2016). B) Histogram of source-
 613 receiver distances using 10 km bins up to 180 km. Note that the number of earthquake source-
 614 receiver pairs in each distance bin is divided by 5 to better enable comparison of the two
 615 distributions.

616

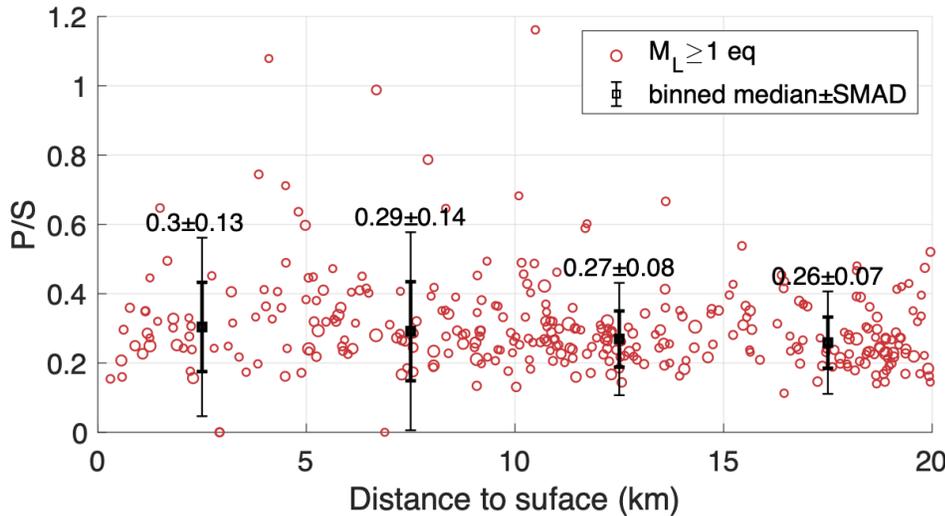


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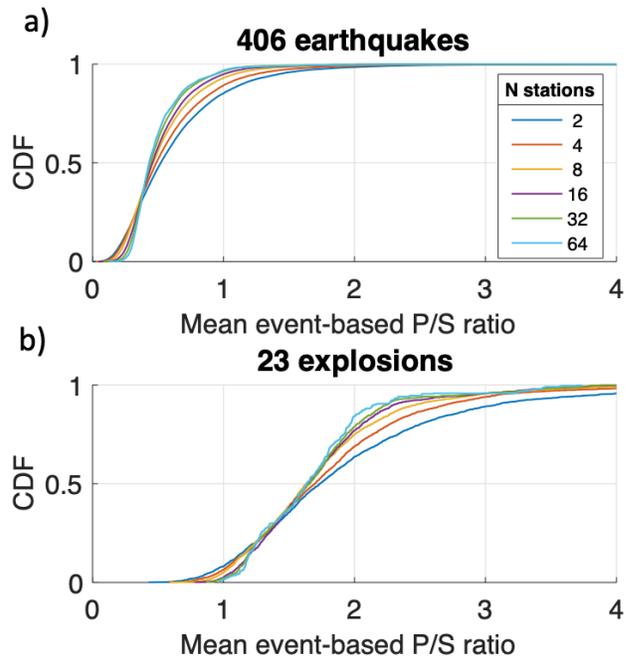
618 Figure 5. Median P/S ratio for explosions and earthquakes at nine different frequency bins: seven
 619 2-Hz narrow bins same as O'Rourke et al., 2016 and two wide bins (filled symbols). Bold error
 620 bars are SMAD and thin bars are 2-scaled median absolute deviation (i.e., 2*SMAD). The
 621 median \pm SMAD for explosions are labeled on top.



622
 623 Figure 6. Distance and magnitude effects. A) P/S versus distance averaged over 20 km with step
 624 size of 20 km for all source-station pairs of earthquakes and explosions. B) P/S ratio versus
 625 magnitudes with bin size of 0.2. Error bars indicate the SMAD calculated from station-based
 626 ratios of all events within each magnitude bin.
 627

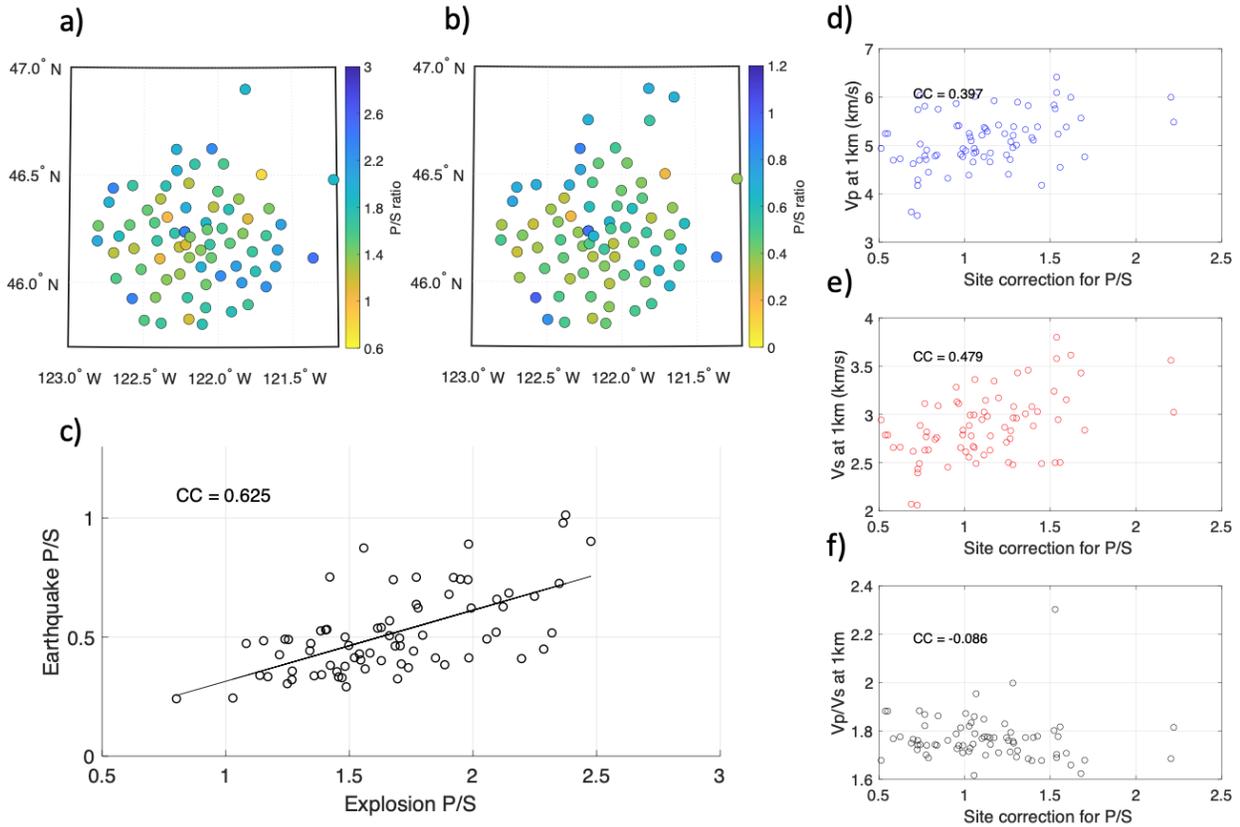


628
 629 Figure. 7. Earthquake P/S ratios versus source depth below surface. Red circles show array-
 630 averaged P/S ratios for individual earthquakes, with circle size scaled by M_L (1-3.3). The four
 631 bold (thin) bars show median SMAD ($2 \times \text{SMAD}$) within depth bins: 0-5 km, 5-10 km, 10-15 km,
 632 and 15-20 km.



633

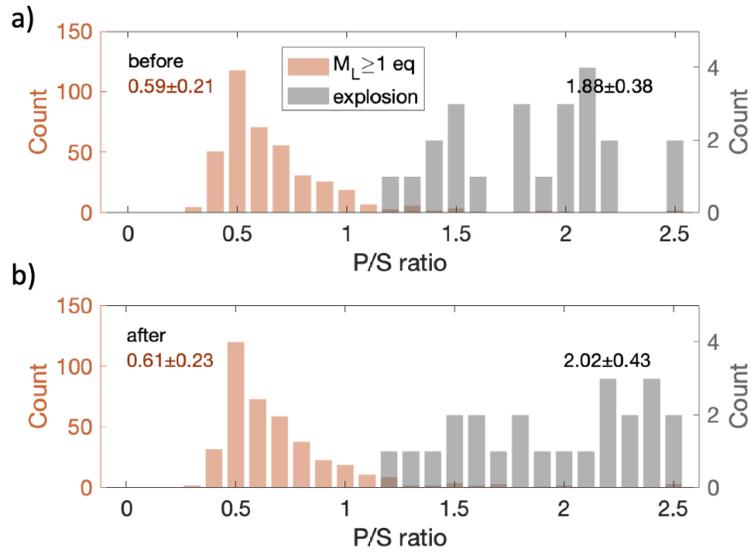
634 Figure 8. Effects of array size on P/S ratios. A) Cumulative distribution functions (CDF) for P/S
 635 ratios of earthquakes as a function of array size for 2, 4, 8, 16, 32, and 64 stations. Each event
 636 ratio is calculated from the median of P/S ratio measured at N stations while the final CDF
 637 curves are generated from the mean of all events. B) Same as (A) except for explosions rather
 638 than earthquakes.



639

640 Figure 9. Site corrections and crustal seismic structure. A) Map of station-averaged P/S ratios for
 641 explosions. B) Map of station-averaged P/S ratios for earthquakes. Note that the color scale is
 642 different from A so that the similarity in spatial pattern is easier to identify. C) Scatter of station-
 643 averaged P/S ratios for earthquakes versus explosions. D-F) Scatter plots of site correction
 644 versus V_p , V_s , and V_p/V_s at 1 km depth from Ulberg et al., 2020. CC: cross-correlation
 645 coefficient.

646

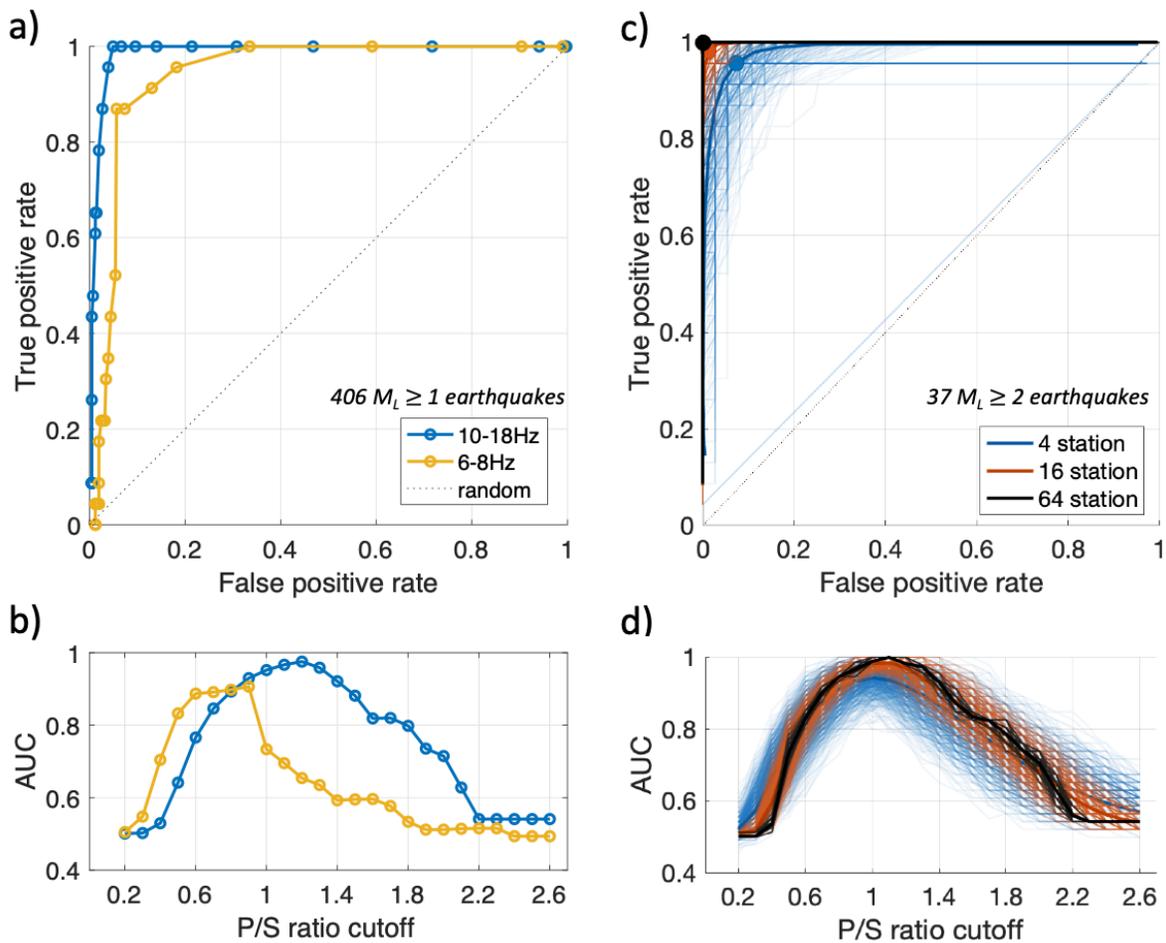


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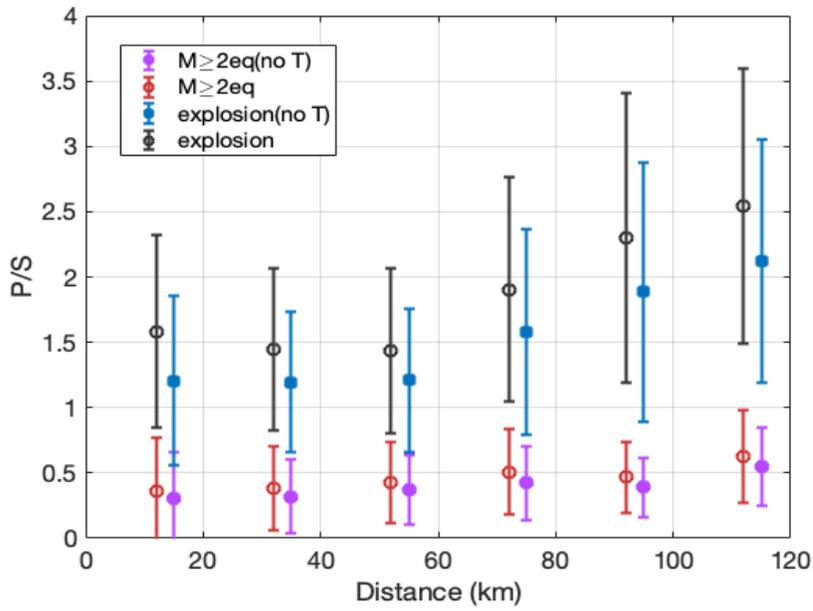
648 Figure 10. Site corrections and P/S ratios. A) Histograms of array-averaged P/S ratios for all

649 explosions and earthquakes. B) Same as A, except the P/S site correction term is applied. The

650 median \pm SMAD of the P/S ratio distributions are labeled in corresponding colors.



651
 652 Figure 11. A) ROC curves for P/S ratio threshold optimization at 10-18 Hz and 6-8 Hz. B) Area
 653 under curve (AUC) for searched P/S ratio thresholds (0.1 step size from 0.2 to 2.6). The
 654 preferred P/S ratio cutoff is 1.2 at 10-18Hz (AUC=0.98), which leads to a true positive rate of
 655 100% and false positive rate of 4.93%. C&D) Similar to A&B) but showing bootstrapping results
 656 using only $M_L \geq 2$ earthquakes. The bold lines are averaged curves from 1000 subsets and the
 657 three dots mark the highest AUC. Note that a few outliers exhibit near-random performance for
 658 the 4-station case (light blue near the diagonal in C) and a few others may reach AUC=1 while
 659 the averages (bold curves) are below 1 for 4-station and 16-station cases (in D).



660

661 Figure 12. Effect of transverse component P-wave energy on P/S ratios. The error bars show
 662 medians and SMAD values of 10-18 Hz P/S ratios in 20 km bins for all source-station pairs
 663 (similar to Figure 6a but using only $M_L \geq 2$ earthquakes and all explosions).

664