

1 Seismic discrimination of controlled explosions and earthquakes  
2 near Mount St. Helens using P/S ratios

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10 **Key Points:**

11 1. Influences on local P/S ratios are analyzed with 23 shallowly buried explosions and 406  $M_L \geq 1$   
12 earthquakes near Mount St. Helens.

13 2. Optimized array-median P/S ratios achieve  $\geq 98\%$  true positives and  $\leq 6.3\%$  false positives  
14 when using  $\geq 16$  stations to classify explosions.

15 3. P/S ratio variations at individual stations are interpreted as site effects that correlate with  
16 shallow crustal velocity structure.

17

## 18 Abstract

19 Explosions and earthquakes are effectively discriminated by P/S amplitude ratios for moderate  
20 magnitude events ( $M \geq 4$ ) observed at regional to teleseismic distances ( $\geq 200$  km). It is less clear  
21 if P/S ratios are effective explosion discriminants for lower magnitudes observed at shorter  
22 distances. We report new tests of P/S discrimination using a dense seismic array in a continental  
23 volcanic arc setting near Mount St. Helens, with 23 single-fired borehole explosions ( $M_L$  0.9-2.3)  
24 and 406 earthquakes ( $M_L$  1-3.3). The array provides up to 95 three-component broadband  
25 seismographs and most source-receiver distances are  $< 120$  km. Additional insight is provided by  
26  $\sim 3,000$  vertical component geophone recordings of each explosion. Potential controls on local  
27 distance P/S ratios are investigated, including: frequency range, distance, magnitude, source  
28 depth, number of seismographs, and site effects. A frequency band of about 10-18 Hz performs  
29 better than lower or narrower bands because explosion-induced S-wave amplitudes diminish  
30 relative to P for higher frequencies. Source depth and magnitude exhibited weak influences on P/  
31 S ratios. Site responses for earthquakes and explosions are correlated with each other and with  
32 shallow crustal  $V_p$  and  $V_s$  from travel-time tomography. Overall, the results indicate high  
33 potential for local distance P/S explosion discrimination in a continental volcanic arc setting,  
34 with  $\geq 98\%$  true positives and  $\leq 6.3\%$  false positives when using the array median from  $\geq 16$   
35 stations. Performance is reduced for smaller arrays, especially those with  $\leq 4$  stations, thereby  
36 emphasizing the importance of array data for discrimination of low magnitude explosions.

## 37 Plain Language Summary

38 Methods to remotely classify seismic sources as either shear-slip earthquakes or shallow  
39 subsurface explosions are important geophysical tools. They are used for investigations of  
40 anthropogenic processes such as underground nuclear explosion tests and mining activity as well  
41 as to obtain pure catalogs of tectonic and volcanic earthquakes. The ratio of compressional (P)  
42 wave amplitude to shear (S) wave amplitude is effective for classifying large earthquakes and  
43 explosions observed hundreds to thousands of kilometers away. Application of such methods at  
44 local distances is a topic of growing interest because smaller magnitude sources are only  
45 observed at close distances. We tested influences on P/S amplitude ratios and their effectiveness

46 for source discrimination using a data set of tectonic and volcanic earthquakes and controlled  
47 shallow borehole explosions near Mount St. Helens. Most observations were within 120 km. We  
48 found that use of high frequencies and array-median statistics is largely effective for source  
49 discrimination in this setting, successfully classifying 100% of explosions while falsely  
50 attributing about 5% of earthquakes to explosions. Variability of P/S ratios across the seismic  
51 array has a highly similar pattern for explosions and earthquakes and that pattern appears to be  
52 controlled by the seismic velocity structure of the shallow crust.

## 53 1. Introduction

54 Quantifying the distinctive properties of explosive seismic sources is an important capability for  
55 identification and characterization of underground nuclear explosion tests and a key component  
56 of verifying compliance with nuclear test-ban treaties (Bowers and Selby, 2009). Seismic  
57 identification and characterization of explosions are also important in other contexts, such as  
58 investigations of chemical explosions that may be the subjects of judicial investigations (e.g.,  
59 Holzer et al., 1996; Koper et al., 2002, 2003) and volcanic explosions studied in the interest of  
60 natural hazard mitigation (e.g., Neuberg et al., 1994; Rowe et al., 1998; Johnson and Lees, 2000).  
61 Early research on seismic discrimination of nuclear explosions and earthquakes focused on  
62 events that are observable at regional to teleseismic distances ( $\geq 200$  km), which generally  
63 requires  $M \geq 4$  (Richards and Zavales, 1990). One useful seismic approach to discriminating  
64 nuclear explosions and earthquakes at such distances is the measurement of P/S amplitude ratios.  
65 Abundant empirical evidence confirms that large explosions ( $M \geq 4$ ) produce greater P/S  
66 amplitude ratios compared to tectonic earthquakes, although the observed ratios are regionally  
67 heterogeneous (e.g., Taylor et al., 1989; Kim et al., 1993; Walter et al., 1995; Hartse et al., 1997;  
68 Xie and Patton, 1999; Jenkins and Sereno, 2001; He et al., 2018; Walter et al., 2018).

69 Potential expansion of seismic discrimination techniques to local distances and lower  
70 magnitudes (or explosive yields) has become a subject of increasing interest (e.g., Zeiler and  
71 Velasco, 2009; O'Rourke et al., 2016; Kolaj, 2018; Pyle and Walter, 2019; Holt et al., 2019;  
72 Kinter et al., 2020). At local distances and lower magnitudes, methods are usually developed to  
73 discriminate chemical explosions from earthquakes and, in some cases, to differentiate single-  
74 fired explosions from delayed-fired explosions that are common in mining activity (Zeiler and  
75 Velasco, 2009; O'Rourke et al., 2016). Single-fired chemical explosions in boreholes provide a  
76 useful proxy for underground nuclear tests (Stump et al., 1999) and well-documented examples  
77 are available for study on account of geophysical experiments targeting seismic source physics  
78 (e.g., Pyle and Walter, 2019) or imaging of geological structures (e.g., O'Rourke et al., 2016).  
79 There is mixed evidence regarding the effectiveness of P/S discrimination for  $\leq M3$  events at  
80 distances of  $\leq 200$  km. Some empirical investigations report that failure to discriminate between  
81 earthquakes and explosions may be restricted to the shortest distances (e.g.,  $\leq 50$  km in O'Rourke  
82 et al., 2016). Others report sporadic failures across the local distance range, potentially on

83 account of lithologic variability of the crust causing complex source and path effects that are  
84 more subdued at regional to teleseismic distances (e.g., Pyle and Walter, 2019, Kinter et al.,  
85 2020). Further research is needed to address questions such as: Does the complexity of crustal  
86 wave propagation make P/S ratios less diagnostic of explosive sources below a common distance  
87 threshold? Can diminished explosion discrimination performance be overcome by larger seismic  
88 arrays or enhanced local calibration using earthquakes to constrain site and/or path effects? What  
89 are the underlying differences in explosion sources that control discrimination capability at local  
90 distances?

91 We use a data set with dense local distance recordings of earthquakes and single-fired  
92 borehole explosions near Mount St. Helens to gain further insight into the seismic source and  
93 structural properties that control the effectiveness of the P/S ratio explosion discriminant for low  
94 yields (Fig. 1). Important aspects of the data set are its diverse source-receiver paths with most  
95 distances <120 km and its combination of single-fired borehole explosions and earthquakes,  
96 including shallow volcanic seismicity at Mount St. Helens (e.g., Ulberg et al., 2020; Glasgow et  
97 al., 2018). The source-receiver distribution was optimized for 3D structural imaging, so the  
98 sources and receivers are broadly distributed within a radius of about 75 km from Mount St.  
99 Helens. Compared to other data sets with one isolated test site or linear transects of receivers, the  
100 diversity of source-receiver paths helps to isolate the effects of different source types from  
101 specific path and site influences. The inclusion of volcanic earthquakes near Mount St. Helens  
102 offers an interesting comparison because volcanoes often produce more frequent shallow  
103 earthquakes and more variable source mechanisms compared to other geologic settings.

## 104 2. Data

105 This study uses seismic recordings of earthquakes and single-fired chemical explosions in  
106 shallow boreholes (Table S1). The explosions were detonated for the controlled source  
107 component of the iMUSH project to image the magmatic system underlying Mount St. Helens  
108 (Kiser et al., 2016, 2018; Hansen et al., 2016). Eight of the 23 boreholes were loaded with 907 kg  
109 of explosive and the other 15 were loaded with 454 kg (Fig. 1b). The explosives were buried in  
110 shallow boreholes with maximum depths of ~22-28 m and explosives occupying the bottom ~5  
111 m of the boreholes. Earthquake source information from 2014 - 2016 was provided by the Pacific  
112 Northwest Seismic Network, which contributes to the USGS Comprehensive Catalog (ComCat;

113 USGS, 2020). Earthquakes within 75 km of Mount St. Helens with  $M_L \geq 1$  were considered for  
114 the study. Lower magnitude earthquakes are poorly recorded across most of the study area and  
115 would be excluded by the requirement of P wave signal-to-noise (SNR)  $> 2$ . Additionally, using  
116  $M_L \geq 1$  provides a close match to the magnitude range of the explosions ( $M_L$  0.9-2.3; calculated  
117 based on waveform amplitudes instead of yield).

118 The primary seismic waveform data for this study are from the broadband part of the  
119 iMUSH project (e.g., Han et al., 2018; Crosbie et al., 2019; Mann et al., 2019; Ulberg et al.,  
120 2020), which temporarily increased the density of local seismic monitoring. The iMUSH  
121 broadband network (XD 2014-2016) was combined with permanent regional three-component  
122 broadband networks (CC and UW) to create a composite network of up to 95 stations within 75  
123 km of Mount St. Helens (Fig. 1a). Sampling rates vary among the networks. Based on the  
124 minimum sample rate of 40 Hz we limited our analysis to frequencies  $\leq 18$  Hz. Network  
125 information for all the broadband data is provided in Table S1. Examples of explosion and  
126 earthquake record sections from the broadband array are shown in Figure 2. The example events  
127 have equal local magnitudes ( $M_L = 1.9$ ) and they are plotted after application of bandpass filtering  
128 from 2-6 Hz. The explosion source exhibits a stronger P-wave than the earthquake, while the  
129 earthquake exhibits a more prominent S-wave than the explosion (Fig. 2).

130 A secondary source of seismic waveform data is vertical-component geophones deployed  
131 during the iMUSH controlled source imaging experiment (Kiser et al., 2016, 2018; Hansen et al.,  
132 2016). Our analysis of source discrimination using P/S energy focuses on three-component  
133 recordings so we only present record sections from the vertical geophones to illustrate local  
134 phase propagation (Fig. 3). In Figure 3, the geophone seismograms for all 23 explosions (70,944  
135 source-receiver pairs) were sorted into 1 km distance bins and the median envelope in each  
136 distance bin is plotted with trace-normalized amplitude. The high density of recordings illustrates  
137 the existence of the S-wave starting at small distances and extending across the array.  
138 Comparison of the 2-6 Hz envelopes in Figure 3a and 6-18 Hz envelopes in Figure 3b shows  
139 diminished S-wave amplitudes relative to P for higher frequencies. Due to the short duration of  
140 the geophone deployment and movement of most geophones during the experiment, there are  
141 few opportunities for comparison with earthquakes that were recorded across most of the array.  
142 Consequently, we focus on the broadband data from 2014 - 2016 for evaluation of P/S ratio as an  
143 explosion versus earthquake discriminant.

## 144 3. Methods

### 145 3.1 P/S amplitude ratios

146 P/S ratios were measured with an approach similar to that used by O'Rourke et al. (2016). Below  
147 we focus on the subtle differences with respect to use of three-component data and phase  
148 windowing for amplitude measurements. O'Rourke et al. (2016) omitted the transverse  
149 components for P measurements because a 1D isotropic medium should not produce P-wave  
150 energy on the transverse component. In contrast to O'Rourke et al. (2016), we use all three  
151 components for measurements of amplitude in P, S, and pre-event noise windows for both  
152 earthquakes and explosions. P-wave energy is commonly observed on transverse components in  
153 our dataset (Fig. 2), presumably due to out-of-plane scattering.

154 Phase windowing at local distances presents a challenge due to the decreasing separation  
155 of P and S with decreasing distance. To maximize use of the data we scaled the window length  
156 by the S-P time, so that the time window length increases with distance until reaching a fixed  
157 duration. The time window starts at -5% of the S-P time before the phase arrival time (P, S or  
158 Noise) and ends at 50% of the S-P time after the arrival time for shorter source-receiver  
159 distances. At larger distances (i.e., beyond 40 km) a fixed value of 3 sec after the arrival time  
160 (Fig. 4) is used for the end of the measurement window. Stations that are too close to an event  
161 (i.e., produce a S-P time window less than 1 sec) are discarded because they prevent reliable  
162 separation of P and S amplitudes and their arrival times are more variable. Pre-event noise time  
163 windows were sampled starting at 10 sec before the origin time of each explosion or earthquake  
164 source. Our goal is to ensure the maximum phase energy is captured within the windows while  
165 minimizing the contamination from noise or interfering phases. Although the optimization of  
166 phase-windowing is somewhat arbitrary, similar P/S ratio results were achieved in additional  
167 tests with the maximum window length increased to 4, 5, and 6 sec. We focus on the 3 sec  
168 window results for the remainder of the text.

169 The phase windows shown in Figure 4 were calculated using a local 1D P and S velocity  
170 model derived from the controlled source survey (Fig. 1b and Fig. S1; Kiser et al., 2016). Events  
171 with P-wave root-mean-square amplitude  $\text{SNR} > 2$  were retained for P/S ratio measurements (Fig.  
172 S2). For SNR calculation, we rotated the data into the LQT reference frame (Vinnik, 1977) and

173 measured P-wave SNR on the L component so that changes in P-wave incidence angle do not  
174 systematically bias the SNR. A minimum SNR value is not required for S-waves because we do  
175 not want to cull weak S-waves expected for explosions. Stability in the results for different phase  
176 window lengths from 3-6 sec indicates that the deviations from the predicted 1D arrival times  
177 have little effect. This is not surprising because phase picks for the explosion sources from  
178 Ulberg et al., (2020) have small travel time residuals compared to the 3 sec window length (Fig.  
179 4). Residual times for 1309 manually picked P phases from explosions recorded by the  
180 broadband array have a standard deviation of 0.3 sec (average 0.01 sec), much smaller than our  
181 window width. Manual picks are unavailable for many P and S phases at individual stations  
182 because only the clearest arrivals are picked. Thus, we prefer the generic phase windowing  
183 approach using the 1D velocity model and 3 sec phase windows for consistency and to avoid  
184 biasing amplitude measurements by under-representing weak S-waves that are important to  
185 source discrimination.

186 After phase windowing the three-component P/S ratio ( $R$ ) at a given station ( $n$ ) was  
187 calculated as:

$$188 \quad R_n = \sqrt{\frac{P_{RTZ}}{S_{RTZ}}}, \text{ Eq(1)}$$

189 where the subscript RTZ (could also be LQT etc.) denotes the three seismogram components and  
190 the summations reflect the total energy within phase windows (P, S or N). All vectors in Eq(1)  
191 have same numbers of elements (i.e., window length). For source discrimination tests, the array  
192 median and scaled median absolute deviation (SMAD) of all the individual P/S ratios are used.  
193 P/S ratios were measured with waveforms bandpass filtered in several frequency bands. We  
194 tested narrow frequency bands of 2-4 Hz, 4-6 Hz, 6-8 Hz, 8-10 Hz, 10-12 Hz, 12-14 Hz, and 14-  
195 16 Hz, following O'Rourke et al., (2016). We also tested two broader frequency bands of 6-12  
196 Hz and 10-18 Hz. In each case, a two-pole Butterworth filter was applied to the response-  
197 corrected waveforms after demeaning and detrending.

### 198 **3.2 Bootstrap resampling for different array sizes**

199 The temporary broadband array (XD), in combination with the permanent networks (UW, CC),  
200 provides better seismic sampling than is available for many areas of interest for explosion  
201 monitoring (Fig. 1a). Although up to 95 stations are available during the 2-year period, not all  
202 stations/components are available the entire time and meet the SNR>2 threshold. Within our

203 preferred frequency range (10-18 Hz), the number of stations that are finally used for P/S ratio  
 204 calculation for explosions ranges from 36 to 78, with an average of 66. The average number of  
 205 stations for  $M_L \geq 2$  and  $M_L 1-2$  earthquakes are 72 and 47, respectively. To fully evaluate the  
 206 potential of our preferred method and parameter set, we used bootstrap resampling test to  
 207 simulate results for six subset array sizes: 2, 4, 8, 16, 32, and 64. For each subset, the cumulative  
 208 array was randomly resampled 1,000 times (without replacement) from the 74 common stations  
 209 that recorded all earthquakes and explosions without any prerequisite (i.e., SNR). Within each  
 210 sampled set, the array-median P/S ratio for earthquakes and explosions are calculated after  
 211 applying the SNR control. In the other words, the bootstrapping approach attempts to simulate  
 212 scenarios with smaller arrays and an unconditioned distribution of SNR recordings.

### 213 **3.3 Site corrections for P/S ratios**

214 Site corrections are often applied to P/S ratio-based discrimination measurements to minimize  
 215 the effects of structural heterogeneity near individual stations (e.g., Walter et al., 1995) because  
 216 the fine-scale structure that influences high-frequency amplitudes is usually not well constrained  
 217 by tomography models. Benefiting from the large number of broadly distributed stations in the  
 218 study area, we estimated station-based site corrections using P/S ratios of earthquakes. This was  
 219 chosen to mimic the circumstance in which P/S corrections could be estimated using only  
 220 earthquake data and then applied to subsequent events of unknown physical origin. The  
 221 correction is calculated as a normalization of event-averaged P/S ratio at each of the N stations:

$$222 \quad C_{1,2,3\dots N} = R_{eq@station(1,2,3,..n)} / \text{mean}(R_{eq@station(1,2,3,..n)}), \quad \text{Eq(2)}$$

223 Where,  $R_{eq@station(1,2,3,..n)}$  is a vector that contains N values, each corresponding to an event-  
 224 averaged P/S ratio (i.e., calculated from up to 406 earthquakes) at a given station after the SNR  
 225 control. For each event (explosion or earthquake) recorded at a subset of m stations, its P/S ratio  
 226 is then corrected by dividing  $C_{1,2,3\dots m}$ . The outcome of site correction is discussed in section 4.5  
 227 and  $R_{eq}$  for the entire array is presented in Figure 9b.

## 228 4. Results

### 229 4.1 Optimal frequency content

230 Array median P/S ratios for explosions are greater than for earthquakes in all frequency bands  
231 (Fig. 5). However, the one SMAD intervals of P/S ratios overlap for lower frequency bands and  
232 most narrow frequency bands. Distributions of P/S ratios are typically not Gaussian (i.e., long-  
233 tailed), so the SMAD and median values are preferred instead of the standard deviation. In  
234 general, higher bands provide larger separation in the median P/S ratios between earthquakes and  
235 explosions, while broader bands help to decrease the variance and stabilize discrimination of  
236 individual events (Fig. 5). With respect to source discrimination, 10-18 Hz is the preferred  
237 frequency band for this local distance data set and it is used for all the results, except where  
238 another frequency band is specifically mentioned. The 14-16 Hz band also performs well but for  
239 individual events it is more variable and it would reduce the number of SNR>2 phase windows  
240 for analysis. The 10-18 Hz array-median P/S ratios and SMAD values for earthquakes and  
241 explosions are  $1.72(\pm 0.34)$  and  $0.46(\pm 0.19)$ , respectively. P/S ratios for both earthquakes and  
242 explosions increase with frequency, however the increase with frequency is greater for the  
243 explosions (Fig. 5). This result from analysis of the three-component broadband array data is  
244 consistent with the observation from the vertical-component geophones showing that S-wave  
245 amplitude diminishes relative to P for higher frequencies (Fig. 3).

### 246 4.2 Distance, magnitude, and depth effects

247 We focus on results from distances <120 km because most of the available source-receiver pairs  
248 are within that distance range (Fig. 4b). Median P/S ratios for earthquakes and explosions sorted  
249 into six 20 km wide distance bins show little change at distances less than ~60 km and then  
250 increasing P/S ratio with distance beyond ~60 km (Fig. 6a). The SMAD values are also larger at  
251 greater distances due to the decreased number of samples within each distance bin. Given that  
252 distance distributions of earthquakes and explosions are very similar in this study (Fig. 4b), we  
253 do not apply distance corrections to the P/S ratios.

254 P/S ratios for earthquakes and explosions do not vary strongly with local magnitude (Fig.  
255 6b). The median P/S ratios in most 0.2  $M_L$  bins overlap within one SMAD. There appears to be

256 an increase in P/S ratio for the largest explosion magnitude bin, but it is heavily influenced by  
257 one explosion source with a particularly high P/S ratio resulting in a relatively large SMAD for  
258 the highest magnitude bin among explosions (Fig. 5b). Earthquake P/S ratios remain low across  
259 the local magnitude range. There is a slight decrease in the median earthquake P/S ratios for the  
260 largest magnitudes ( $M_L > 2.5$ ), which is within the range of one SMAD. Given the weak distance  
261 and magnitude dependences found in the P/S ratios, we did not apply the magnitude and distance  
262 amplitude correction (MDAC) approach that is commonly used in regional distance studies  
263 (Walter and Taylor 2001; Anderson et al., 2009).

264 Estimated earthquake source depths exhibit weak correlation with P/S ratios (Fig. 7). As  
265 the area near Mount St. Helens is characterized by variable surface topography (i.e., ranging  
266 from 0 - 4 km, Fig. 1). To account for elevation in Figure 7, we add the surface elevations at  
267 event epicenter locations to the source depths reported relative to sea level. The sum thus reflects  
268 the distances between the hypocenters and the surface. Binning the earthquake sources into four  
269 depth ranges (0-5, 5-10, 10-15, and 15-20 km) results in median P/S ratios that all overlap within  
270 one SMAD. Depth uncertainties are highly variable depending on local array coverage, but  
271 reported uncertainties from the Pacific Northwest Seismic Network for  $M_L \geq 1$  earthquakes near  
272 Mount St. Helens are typically  $< 1$  km. In that context, results from binning within 5-km depth  
273 intervals should not be strongly biased by inaccurate depth estimates. There is a slight decrease  
274 in median P/S ratio from 0.78 at 0-5 km to 0.41 at 15-20 km, which is comparable to the SMAD  
275 (i.e., 0.1-0.35) for any of the source depth bins.

### 276 **4.3 Number of stations in the seismic array**

277 Bootstrap resampling of the three-component seismographs simulates the potential average  
278 source discrimination performance with smaller seismic arrays (see section 3.2). The cumulative  
279 distribution functions (CDFs) from resampling show that greater variations are observed for  
280 explosion P/S ratios compared to earthquake P/S ratios (Fig. 8). Increasingly large seismic arrays  
281 help reduce the overlap of earthquake and explosion P/S ratio distributions near a value of  $\sim 1$   
282 (Fig. 8). Separation of earthquake and explosion P/S ratios is subject to diminishing  
283 improvement for arrays with over 16 stations. The improvement with increasing array size  
284 appears modest in this context because the curves shown in Figure 8 are generated as averages  
285 from 1,000 bootstrap resampling subsets (for 2, 4, 8, 16, 32 and 64 station cases). The variance

286 of P/S ratios is much larger for smaller arrays and its effect on discrimination performance is  
287 discussed further in section 5.1.

#### 288 **4.4 Site response effects and shallow crust structure**

289 Variations in station-averaged P/S ratios from earthquakes and borehole explosions exhibit  
290 similar spatial patterns, despite the generally higher P/S ratios for explosions (Fig. 9). A scatter  
291 plot of the earthquake station-averages versus the explosion station-averages shows an  
292 approximately linear trend, with a correlation coefficient of 0.625. If the earthquakes are subset  
293 by magnitude, the  $M_L 1-2$  and  $M_L \geq 2$  subsets yield correlations of 0.625 and 0.641 (these two  
294 earthquake subsets are correlated at 0.91), respectively. These correlations indicate that  
295 observations of small ( $\sim M_L 1-3$ ) earthquakes may provide a useful basis for determining  
296 empirical P/S amplitude site corrections that are applicable to explosions. However, the  
297 improvement for the purpose of source discrimination appears to be subtle in this case (Fig. 10).  
298 Application of site corrections increased the difference between the median explosion and  
299 earthquake P/S ratios from 1.29 to 1.41, but the SMAD values also increased slightly for  
300 explosions (0.38 to 0.43) and earthquakes (0.21 to 0.23). Furthermore, we found the site  
301 correction terms are positively correlated with shallow crustal velocities. We adopt a velocity  
302 model from a recent local travel time tomography study around Mount St. Helens (Ulberg et al.,  
303 2020) and evaluate the correlation of our site corrections with the model. The  $V_p$ ,  $V_s$  and  $V_p/V_s$   
304 values are extracted from the tomography at 1 km depth beneath all the station (site) locations  
305 (i.e., interpolated from the tomography model using each station's latitude and longitude).  
306 Overall, the cross-correlation coefficients for the site correction terms are 0.397 for  $V_p$  and 0.479  
307 for  $V_s$ . Site corrections exhibit a much weaker correlation (-0.086) with  $V_p/V_s$  (Fig. 9 d-f). The  
308 correlation coefficients remain comparable for all layers around sea level ( $\pm 2$  km) and they  
309 decrease at deeper depths, suggesting that the site correction is influenced by uppermost crustal  
310 structure.

## 311 5. Discussion

### 312 **5.1 Effectiveness for explosion discrimination**

313 To evaluate the performance of different frequency bands and array sizes, we adopt receiver  
314 operating characteristic (ROC) curves (James et al., 2013), which show the diagnostic  
315 performance of binary classifiers calculated from: true positive, false positive, true negative, and  
316 false negative results. In this case for explosions versus earthquakes, we treat explosions  
317 identified correctly as “true positive” and earthquakes identified as explosions as “false positive”  
318 (vice versa for earthquakes). For each P/S ratio used as a discrimination threshold, the point  
319 along the ROC curve is determined by the rate of true positives and false positives. The optimal  
320 discrimination threshold is chosen by maximizing the area under the ROC curve (AUC). Thus,  
321 an ideal classifier would be plotted in the upper left corner corresponding to 100% true positive  
322 and 0% false positives. Application to P/S ratios with the preferred frequency band of 10-18 Hz  
323 and the full data set of earthquakes and explosions shows 100% true positives and 4.93% (20 out  
324 of 406) false positives for a P/S ratio threshold of 1.2 (Fig. 11a). Half of the events that create  
325 false positives (i.e.,  $P/S > 1.2$ ) are only recorded with  $< 6$  stations, reflecting the disadvantage of  
326 insufficient station coverage for low-magnitude sources (Fig. S5). For comparison, a lower and  
327 narrower frequency band of 6-8 Hz results in 86.95% true positives and 5.67% false positives for  
328 a P/S ratio threshold of 0.9 (Fig. 11b).

329 Discrimination performance generally improves with increasing event magnitude and  
330 array size (Fig. 11c, d). Using all explosions and only  $M_L \geq 2$  earthquakes, a threshold P/S ratio of  
331 1.2 results in 100% true positives and 0% false positives. The  $M_L$  0.9-2.3 explosions produced an  
332 average of 66 stations with  $SNR > 2$ , while the  $M_L$  1-2 earthquakes only produced an average of  
333 47 stations with  $SNR > 2$ . So, the diminished discrimination performance for  $M_L$  1-2 earthquakes  
334 is likely influenced by SNR at individual stations and the total number of stations available for  
335 analysis. ROC curves for seismic arrays composed of  $N=4$ , 16, and 64 seismographs illustrate  
336 the effects of array size (Fig. 11c). For  $N=64$ , the bootstrap resampling results show that a  
337 maximum AUC of 1 is consistently achieved for discrimination of explosions and  $M_L \geq 2$   
338 earthquakes. For  $N=16$ , the average of the AUC maxima is 0.98. For  $N=4$ , the average of the  
339 AUC maxima reduces to 0.94 (Fig. 11d). However, the ROC curves for  $N=4$  are much more

340 variable, including a few samples with near-random performance (Fig. 11c) and some extreme  
341 cases reaching the AUC maximum (Fig. 11d). Generally, larger array size is expected to better  
342 mitigate source and path variations, so the requirement could be much lower in the case where  
343 the explosion and earthquake sources are co-located. A separate bootstrap resampling test with  
344 an earthquake epicenter nearly co-located with an explosion shows that <16 stations are  
345 sufficient for robust discrimination (Fig. S6), suggesting that the minimum number of stations  
346 could be much lower if the earthquake epicenter and suspected explosion are closely located. In  
347 this example the horizontal locations are separated by 2.4 km and the depths are separated by  
348 11.1 km.

349         Comparison of the new results from near Mount St. Helens with other local distance P/S  
350 ratio discrimination tests may be influenced by different local propagation effects related to  
351 geological settings as well as measurement approaches. A similar scale study using data covering  
352 the Bighorn mountain range and adjacent sedimentary basins in Wyoming found effective P/S  
353 discrimination at ~50-200 km distance but failure at <50 km distance (O'Rourke et al., 2016). As  
354 our analysis exhibits effective discrimination at such distances, below we consider two minor  
355 methodological differences between this study and O'Rourke et al. (2016) that might contribute  
356 to the difference in performance. We acknowledge that different local propagation effects may  
357 also be the cause of the difference in discrimination performance, but a thorough re-analysis of  
358 their data would be required to isolate that influence.

359         The first methodological difference is that we include the transverse component for P-  
360 wave measurements (see section 3.1). Explosion recordings in this study commonly show  
361 SNR>2 (our threshold for analysis) even for P-waves recorded on the transverse component (Fig.  
362 2). If scattering of P energy onto the transverse component is important at distances <50 km, then  
363 the inclusion of transverse component data may be beneficial for explosion discrimination. A  
364 comparison of array-median P/S ratios with and without the transverse component shows that  
365 separation of the explosion and earthquake ratios improves with inclusion of the transverse  
366 component (Fig. 12). The increased separation is primarily due to increases in the explosion P/S  
367 ratios, while changes in the earthquake P/S ratios are smaller. This is consistent with the  
368 possibility that out-of-plane P-wave scattering is stronger for explosions than earthquakes. In this  
369 case, the benefit of including transverse component P-wave energy spans our entire local

370 distance range (Fig. 12), but given that P/S ratios tend to increase with distance for both  
371 approaches the incremental improvement is more important at smaller distances ( $\leq 60$  km).

372 The second difference is that we did not apply the MDAC method for regional seismic  
373 discriminants (Walter and Taylor 2001; Anderson et al., 2009) to correct for distance and  
374 magnitude effects. We chose not to use MDAC because the distance and especially magnitude  
375 trends in our raw P/S ratios are modest compared to the SMAD values for explosion and  
376 earthquakes, respectively (Fig. 6). Additionally, MDAC was originally designed for larger  
377 distances (e.g.,  $>100$  km) and O'Rourke et al. (2016) note that stations at their shortest distances  
378 ( $\sim 20$ - $40$  km) exhibit abnormally high MDAC corrections for explosions, further challenging  
379 their discrimination. We speculate that the amplitude correction techniques developed for  
380 regional distances may need to be revised for shorter local distances. Similar to the weak  
381 distance and magnitude trends found in this study, Zeiler and Velasco (2009) reported negligible  
382 distance dependence of explosion discriminants (including P/S ratios) within the local distance  
383 range. We suggest that the necessity and design of the amplitude correction techniques for  
384 explosions observed at short distances ( $\leq 50$  km) should be further investigated.

385 In a recent local to regional distance study, Pyle and Walter (2019) investigated P/S ratio  
386 discrimination with six chemical explosions from the Source Physics Experiment (Snelson et al.,  
387 2013) and nearby tectonic earthquakes. Similar to O'Rourke et al. (2016) and this study, Pyle  
388 and Walter (2019) found that P/S discrimination performance improved with increasing  
389 frequency ( $\geq 6$  Hz) and that array averaging of  $\sim 10$  or more stations was needed to achieve clear  
390 separation of explosion and earthquake P/S ratios. Four of the six explosions used in their study  
391 had larger explosive yields than all the explosions in this study and the receiver spacing within  
392  $\sim 100$  km was sparser, so relative to O'Rourke et al., (2016) there is less opportunity for  
393 comparison of results at similar scales. The fact that we observe optimal performance for  
394 somewhat higher frequencies in this study (e.g., 10-18 Hz) likely reflects our focus on shorter  
395 source-receiver distances of  $<120$  km compared to distances up to  $\sim 450$  km in Pyle and Walter,  
396 (2019).

## 397 **5.2 Source effects**

398 The geophone record sections show that S-waves emerge within the first few kilometers from the  
399 source, acknowledging that there is not sufficient sampling available to resolve S-wave

400 emergence in detail at scales of hundreds of meters (or less) from the source (Fig. 3). Assuming  
401 the S-wave is effectively generated at the source for this data set, increasing P/S ratio with  
402 distance is expected if S-wave attenuation is greater than P-wave attenuation in the crust (e.g.,  
403 Pyle et al., 2017). In contrast, a difference in source spectra may be needed to explain why  
404 explosion P/S ratios increase with frequency more than earthquake P/S ratios (Fig. 5).

405         Prior studies of  $M \geq 3$  chemical explosions and nuclear explosions indicate that explosion-  
406 induced crustal S-waves (Lg) exhibit lower corner frequencies than explosion-induced P-waves  
407 (local Pg & regional Pn phases; Xie, 2002; Fisk, 2006, 2007). In these studies, the S-wave corner  
408 frequency is typically about half of the P-wave corner frequency. Our results with lower yield  
409 chemical explosions are similar based on the increased separation of local distance explosion and  
410 earthquake P/S ratios at higher frequencies. The 10-18 Hz band may perform relatively well for  
411 P/S ratio discrimination because it partially overlaps the interval between the lower S-wave  
412 corner frequency and the higher P-wave corner frequency (e.g., Fisk, 2007). Using the Mueller-  
413 Murphy model corner frequency scaling from Fisk, (2007) the explosions in this study are  
414 expected to produce local P-wave corner frequencies of  $\sim 35$ -45 Hz and S-wave corner  
415 frequencies of  $\sim 17$ -23 Hz. The 40 Hz sampling rate for most stations limited our analysis to  
416 frequencies below  $\sim 18$  Hz, so only the highest frequencies in this study are near the expected S-  
417 wave corner. Extension of P/S ratio measurements to higher frequencies by collecting higher  
418 sample-rate data may be beneficial, especially for very short distances ( $\leq 50$  km) and low  
419 magnitudes ( $M_L \leq 2$ ).

420         The physical controls on explosion-induced S-wave spectra remain debated. If a  
421 difference in source spectra explains the observed frequency dependence of P/S ratios, the  
422 physical cause may be rooted in the different P- and S-wave elastic length scales of sensitivity to  
423 near-source rock damage (Taylor, 2009). However, a variety of complicated and locally specific  
424 effects such as spall and free-surface topographic scattering are thought to influence explosion-  
425 induced S-wave spectra (e.g., Xie and Lay, 1994; Patton and Taylor, 1995). Multiple explosion  
426 source studies suggest that the conversion from Rayleigh to S-wave could be the dominant  
427 contributor to explosion S-waves and control the distinct frequency-dependent decay of S-wave  
428 amplitudes (e.g., Myers et al., 1999; Pitiraka et al., 2015; Mellors et al., 2018). An alternative to  
429 explaining the frequency dependence of P/S ratios with different source spectra is that explosions  
430 may preferentially excite shallower shear modes that attenuate more rapidly with distance (e.g.,

431 Baker et al., 2004, 2012). Regardless of the exact S-wave excitation mechanism, our results  
432 show that local distance P/S ratios increase with frequency; the effects of both source diversity  
433 and near-source structural complexity, even around an active volcano, can be suppressed using  
434 array median P/S ratios if the array size is large enough.

435 One explosion source in this study that produced a relatively low P/S ratio resulted in  
436 clear surface evidence of shear slip at the source. The ‘X4’ explosion (Fig. 1b; also see Fig. S4  
437 and Table S1) detonated in a borehole with maximum depth of ~22 m depth resulted in a small  
438 normal fault scarp with a length of ~15 m and vertical offset of up to ~20 cm. Consequently, it is  
439 unsurprising that this explosion exhibited a relatively low P/S ratio of 1.27 (Fig. 10), which is  
440 near the optimal binary classification cutoff of 1.2 for the 10-18 Hz data set including all  
441  $M_L \geq 1$  earthquakes (Fig. 11b). It is unknown if ‘blind’ shear failures that did not rupture the  
442 surface are common for other low P/S ratio explosions.

### 443 **5.3 Combining local distance seismic discriminants**

444 The P/S ratio results presented here show the potential for effective discrimination if a large local  
445 array is available, but in practice explosion discrimination is usually more challenging due to  
446 smaller arrays and source discrimination relies on evidence from multiple types of seismic  
447 measurements. Consequently, we discuss possibilities for combining P/S ratios with other types  
448 of local distance source discriminants. Ratios of different seismic magnitude metrics such as mb  
449 (body-wave magnitude) &  $M_s$  (surface-wave magnitude) have long been used as an initial or  
450 ‘screening’ step for source discrimination of  $M \geq 3$  events (Stevens and Day, 1985; Selby et al.,  
451 2012; Ford and Walter, 2014). At local scales there is growing evidence that the difference  
452 between the local (Richter) magnitude and the coda duration magnitude ( $M_L - M_C$ ) can help  
453 discriminate explosions, primarily because the magnitude difference is sensitive to source depth  
454 (Holt et al., 2019; Voyles et al., 2020).  $M_L$  and  $M_C$  measurements are based on different parts of  
455 the seismogram.  $M_L$  is controlled by the peak seismic amplitude, while  $M_C$  is controlled by the  
456 duration of later-arriving scattered energy. Very shallow sources such as borehole explosions  
457 preferentially produce longer coda leading to negative  $M_L - M_C$ . P/S amplitude ratios, as  
458 implemented in this study, ignore the extended coda and we find weak source depth dependence  
459 for P/S amplitude ratios (Fig. 7). Thus, the capabilities of the two discriminants may be rooted in  
460 complementary aspects of the local seismic wavefield. A simple workflow to leverage the two

461 approaches would be using  $M_L$ - $M_C$  to screen for unusual events given that routine catalog  
462 generation can commonly provide both parameters. Then events identified by screening could be  
463 further investigated with P/S ratios. More thorough approaches to jointly classifying events  
464 based on  $M_L$ - $M_C$  and P/S ratios should also be considered. P/S ratio measurements could also be  
465 automated to enhance screening capabilities once travel time relationships and site corrections  
466 are developed for an array. Additional use of more time-consuming moment tensor analysis of  
467 low magnitude local distance events might be reserved for events flagged by  $M_L$ - $M_C$  and P/S  
468 screening (e.g., Alvizuri and Tape, 2016).

## 469 6. Conclusions

470 P/S ratio discrimination of earthquakes and shallow single-fired borehole explosions at distances  
471 less than 120 km was tested with a dense broadband seismic array near Mount St. Helens. Taking  
472 advantage of the excellent coverage of both stations and sources, we evaluated the effects of  
473 frequency bands, source-receiver distances, source magnitudes and focal depths. Optimal  
474 separation of P/S ratios for the two sources types was found using a 10-18 Hz frequency band,  
475 which achieved explosion discrimination with 100% true positives and 4.93% false positives  
476 using the entire array. Randomly resampling to simulate smaller arrays shows performance of  
477  $\geq 98\%$  true positives and  $\leq 6.3\%$  false positives for  $\geq 16$  stations. Performance becomes highly  
478 variable using  $\leq 4$  stations, likely as a result of structural complexity in the volcanic arc setting.  
479 Successful separation using the dense array and optimized frequency band left limited room to  
480 improve the performance, consequently our site corrections derived from 406 local earthquakes  
481 had a negligible effect on discrimination statistics. Despite the limited improvements in this case,  
482 we found that the site corrections correlate with  $V_p$  and  $V_s$  of the uppermost crust from a recent  
483 tomography study. Future studies using P/S ratios may benefit from local site corrections derived  
484 from small earthquake recordings or local tomography models.

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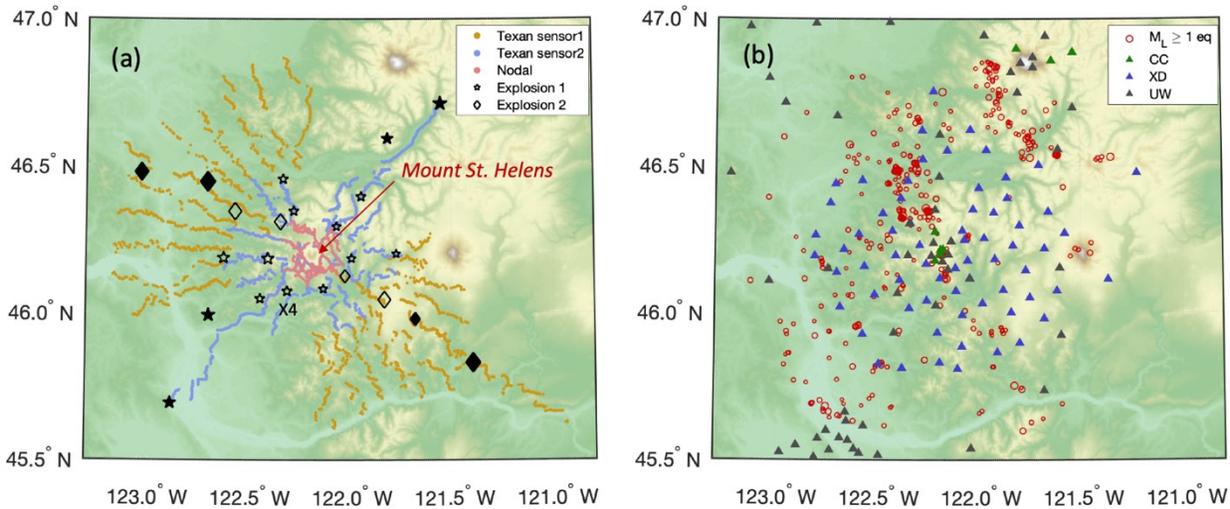
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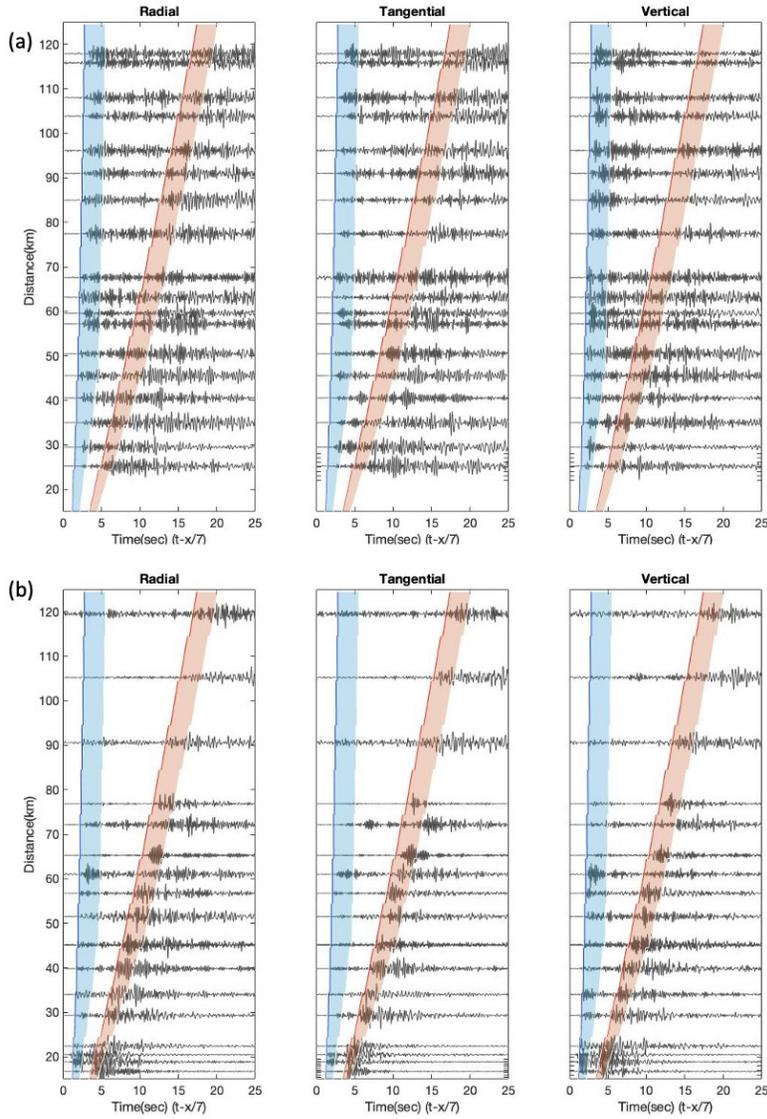
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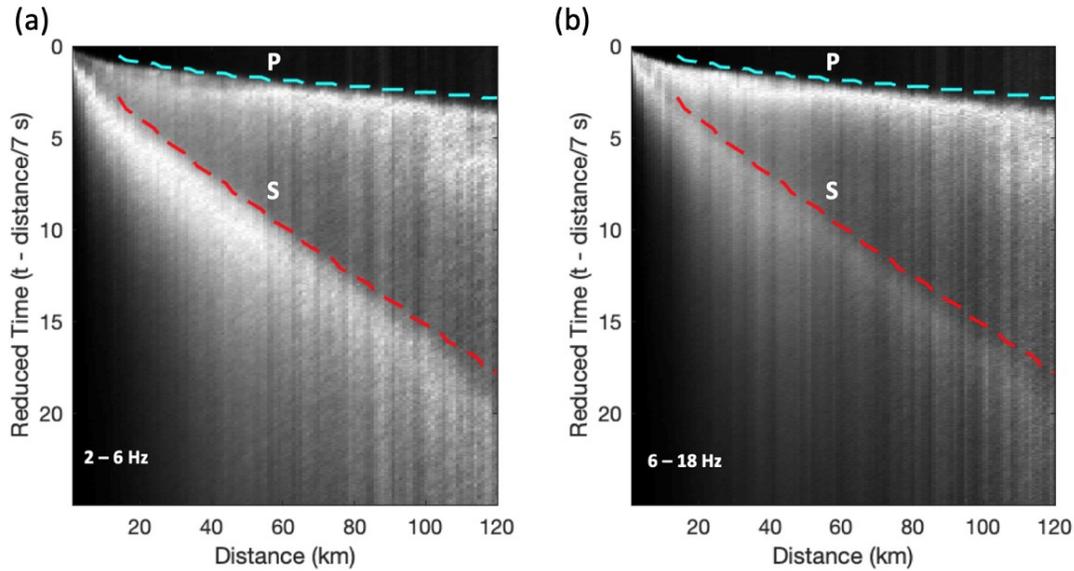
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646 Figure 1. Study area maps with sources and receivers. A) Vertical geophone locations are plotted  
 647 along with single-fired explosion locations. Explosion locations loaded with 907 kg of explosive  
 648 are denoted by filled symbols and locations loaded with 454 kg are denoted by hollow symbols.  
 649 The symbol sizes for explosions are scaled by their  $M_L$ . Explosions labeled with stars were  
 650 detonated during controlled source phase 1 (recorded by Texan 1 array; ~2370 nodes) and  
 651 diamonds were detonated during phase 2 (recorded by Texan 2 array; ~2220 nodes). 'X4'  
 652 denotes one explosion that is discussed in the text. Geophone locations in pink (~900 nodes)  
 653 recorded both sets of explosions. B) Broadband stations used in the study are plotted along with  
 654 the locations of  $M_L \geq 1$  earthquakes that occurred between June 20, 2014 to August 31, 2018)  
 655 within 75 km of Mount St. Helens. The time span corresponds the deployment of XD array  
 656 (blue); permanent stations are shown as CC (green) and UW (grey).



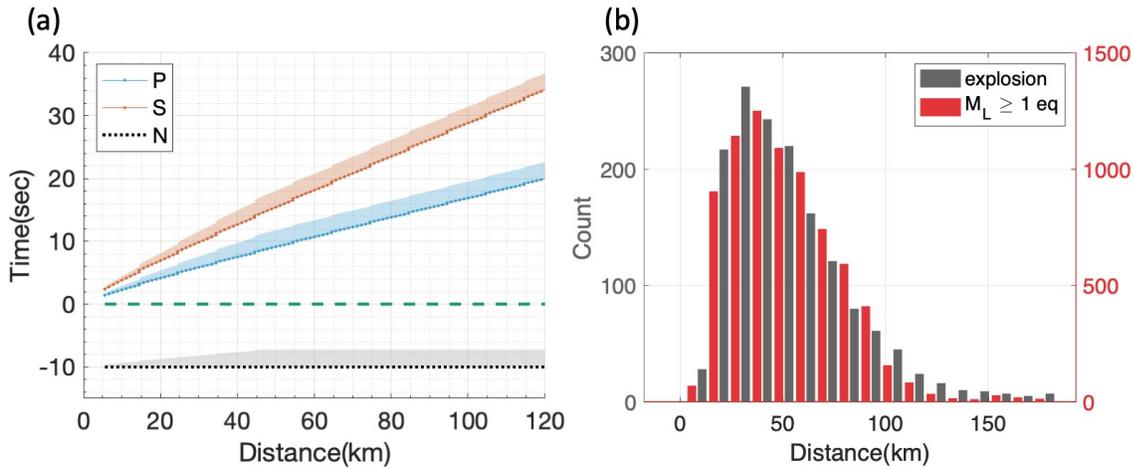
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658 Figure 2. A) A record section is plotted for an explosion event with 616kg equivalent TNT load  
 659 (Y8, located at the NW of array,  $M_L=1.9$ , depth=0 km; see Table S1 for details). The event  
 660 showed relatively strong S energy among explosions. Only 18 seismograms are shown for  
 661 clarity. B) Record section for an equal-magnitude earthquake (2015 Feb 9, 05:45:35, depth=0.4  
 662 km) with waveforms from 19 stations. Waveforms are filtered between 2-6 Hz at plotted with a  
 663 reduced velocity of 7 km/s in both figures. The blue and red shades mark the P and S wave  
 664 windows, predicted using a locally optimized 1D velocity model (Kiser et al., 2016; also see Fig.  
 665 S1 and section 3.1). Note the relatively strong P energy around 60 km. Same events but filtered  
 666 with 10-18 Hz are shown in Fig. S3.



667  
 668 Figure 3. Stacked geophone recordings of explosions. A) Median envelopes of geophone  
 669 seismograms from all 23 explosions in 1 km distance bins (70,944 source-receiver pairs).  
 670 Seismograms were bandpass filtered from 2-6 Hz before envelope calculation and median-  
 671 stacking. Median envelopes at each distance are normalized by their maximum. The cyan dashed  
 672 line marks the beginning of the P window and the red dashed line marks the beginning of the S  
 673 window. B) Same as A, except that seismograms were bandpass filtered from 6-18 Hz. The  
 674 higher frequency band exhibits diminished S-wave amplitudes relative to P.  
 675

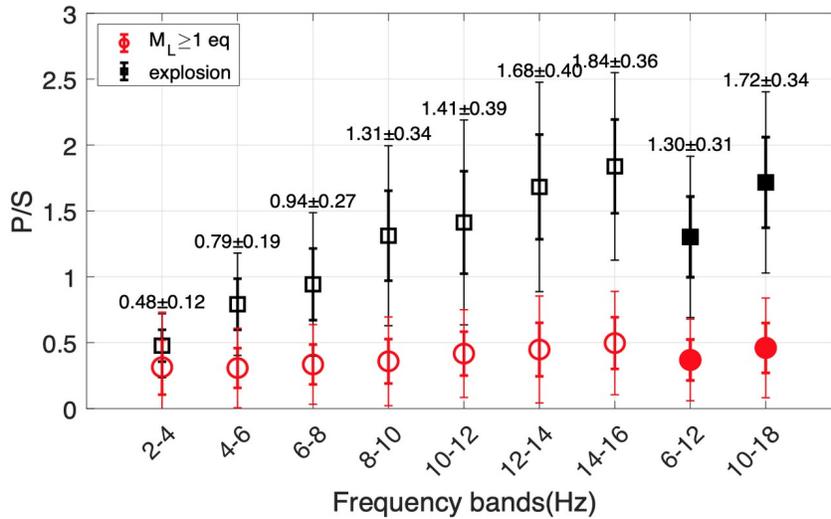
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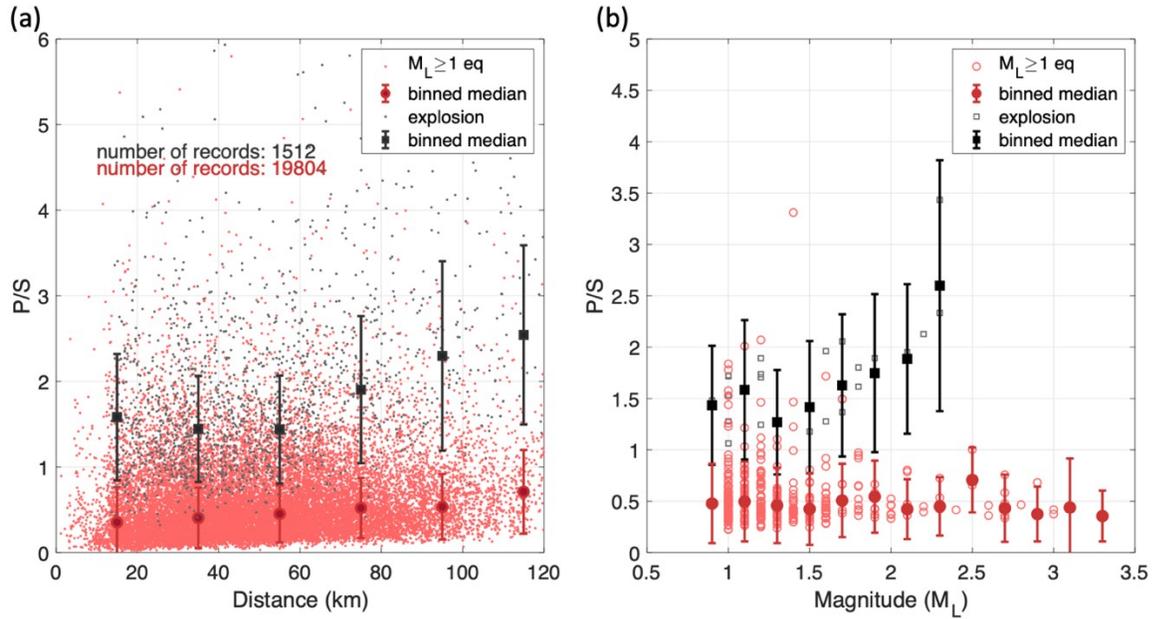
678 Figure 4. Phase windowing and source-receiver distances. A) Phase windowing based on travel  
679 times from a local 1D P and S velocity model (Kiser et al., 2016; also see Fig. S3&4 for  
680 waveform examples). B) Histogram of source-receiver distances using 10 km bins up to 180 km.  
681 Note that the number of earthquake source-receiver pairs in each distance bin is divided by 5 to  
682 better enable comparison of the two distributions.

683

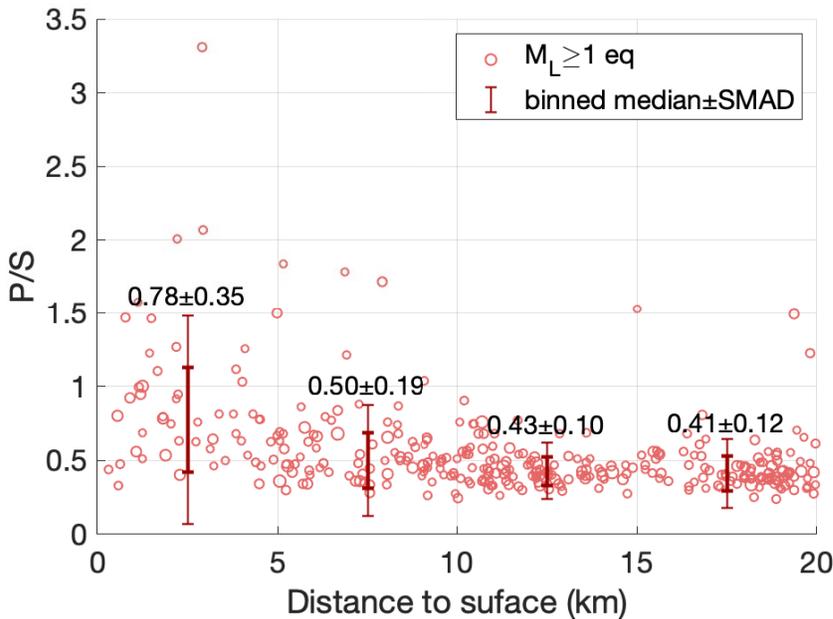


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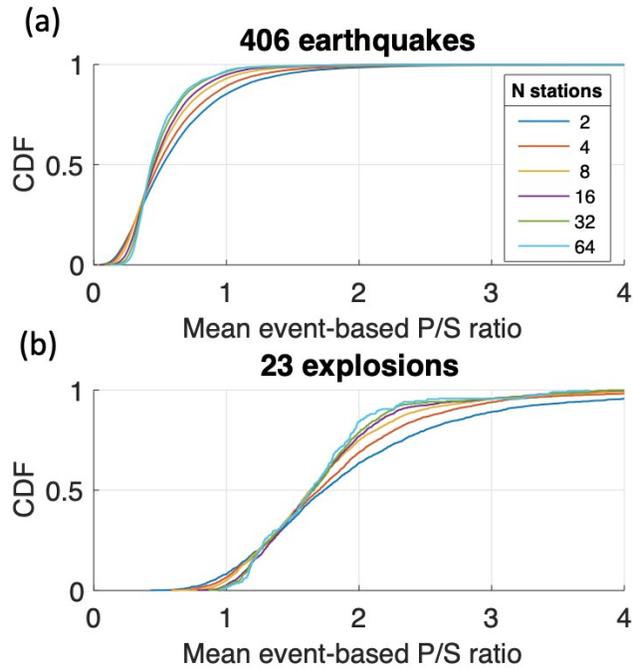
685 Figure 5. Median P/S ratio for explosions and earthquakes at nine different frequency bins: seven  
686 2-Hz narrow bins same as O'Rourke et al., 2016 and two wide bins (filled symbols). Bold error  
687 bars are SMAD and thin bars are 2-scaled median absolute deviation (i.e., 2\*SMAD). The  
688 median±SMAD for explosions are labeled on top.



689  
 690 Figure 6. Distance and magnitude effects (calculated at 10-18 Hz). A) P/S versus distance  
 691 averaged over 20 km with step size of 20 km for all source-station pairs of earthquakes and  
 692 explosions. B) P/S ratio versus magnitude with bin size of 0.2. Error bars indicate the SMAD  
 693 calculated from station-based ratios of all events within each magnitude bin.

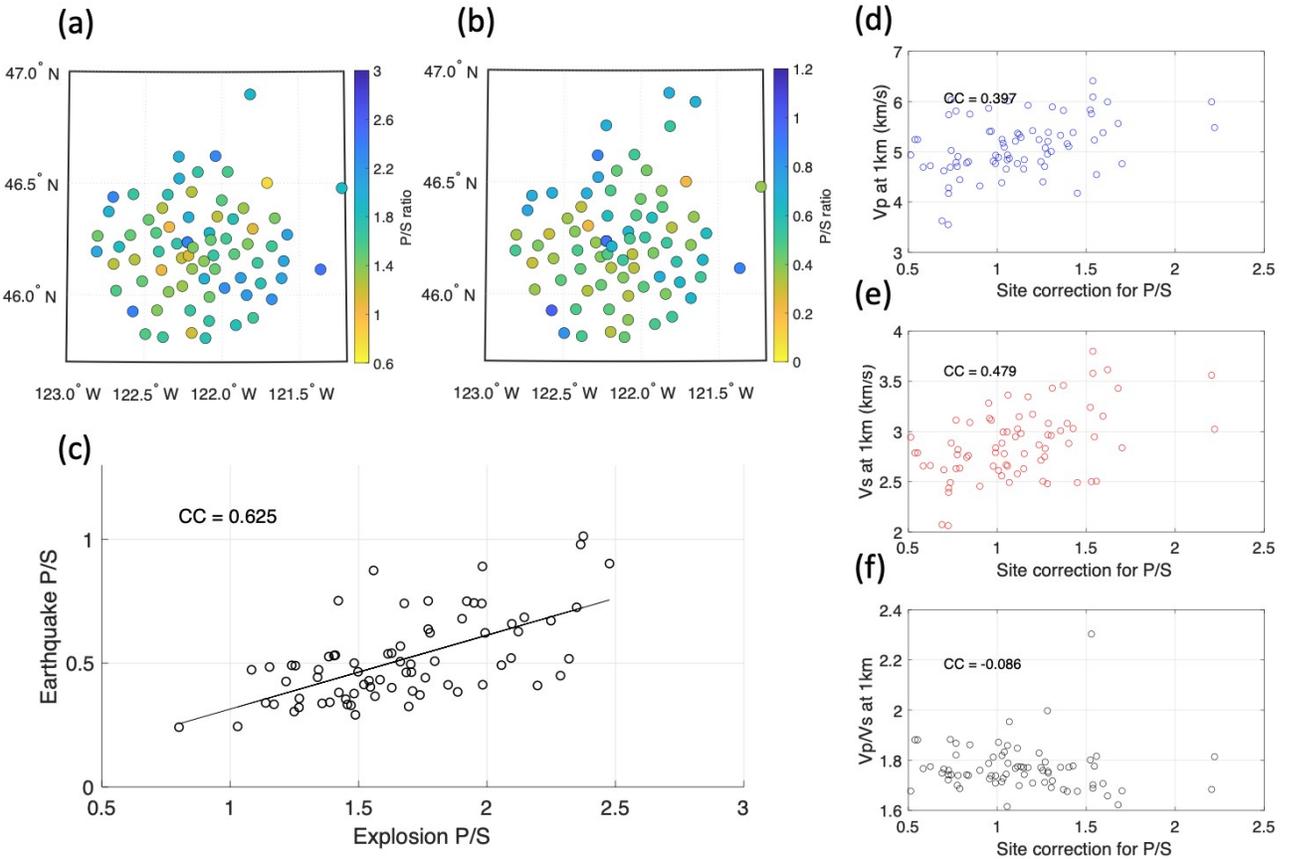


694  
 695 Figure 7. Earthquake P/S ratios versus source depth below surface (calculated at 10-18 Hz). Red  
 696 circles show array-averaged P/S ratios for individual earthquakes, with circle size scaled by  $M_L$   
 697 (1-3.3). The four bold (thin) bars show median SMAD ( $2 \times \text{SMAD}$ ) within depth bins: 0-5 km, 5-  
 698 10 km, 10-15 km, and 15-20 km.



699

700 Figure 8. Effects of array size on P/S ratios (calculated at 10-18 Hz). A) Cumulative distribution  
 701 functions (CDF) for P/S ratios of earthquakes as a function of array size for 2, 4, 8, 16, 32, and  
 702 64 stations. Each event ratio is calculated from the median of P/S ratio measured at N stations  
 703 while the final CDF curves are generated from the mean of all events. B) Same as (A) except for  
 704 explosions rather than earthquakes.



705

706 Figure 9. Site corrections and crustal seismic structure (calculated at 10-18 Hz). A) Map of  
 707 station-averaged P/S ratios for explosions. B) Map of station-averaged P/S ratios for earthquakes.

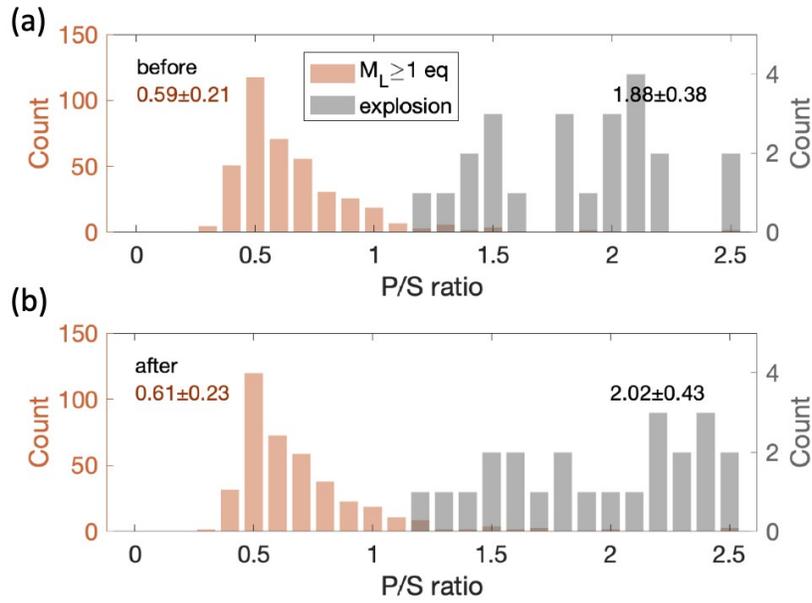
708 Note that the color scale is different from A so that the similarity in spatial pattern is easier to

709 identify. C) Scatter of station-averaged P/S ratios for earthquakes versus explosions. D-F) Scatter

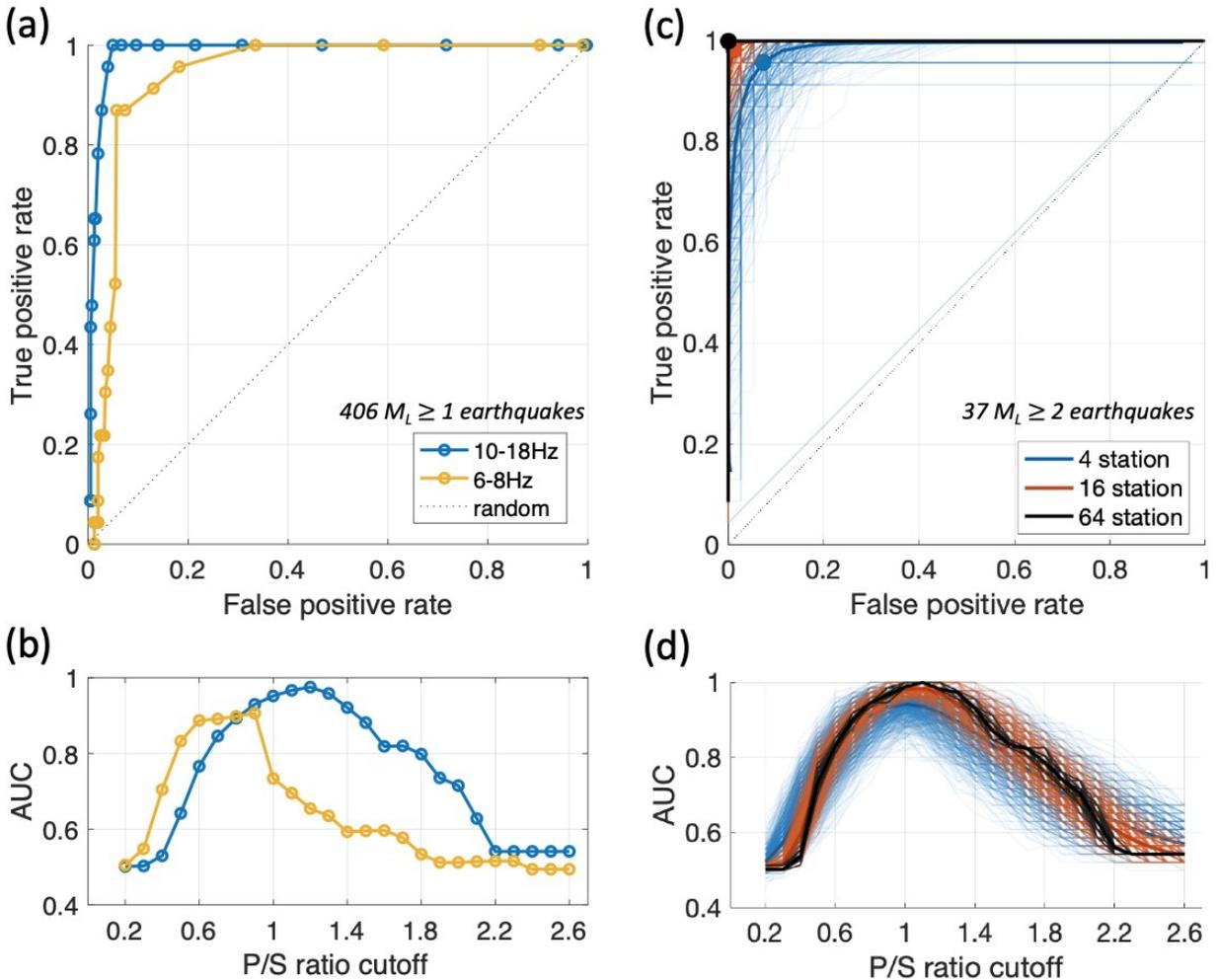
710 plots of site correction versus Vp, Vs, and Vp/Vs at 1 km depth from Ulberg et al., 2020. CC:

711 cross-correlation coefficient.

712



713  
 714 Figure 10. Site corrections and P/S ratios (calculated at 10-18 Hz). A) Histograms of array-  
 715 averaged P/S ratios for all explosions and earthquakes. B) Same as A, except the P/S site  
 716 correction term is applied. The median $\pm$ SMAD of the P/S ratio distributions are labeled in  
 717 corresponding colors.



718

719 Figure 11. A) ROC curves for P/S ratio threshold optimization at 10-18 Hz and 6-8 Hz. B) Area

720 under curve (AUC) for searched P/S ratio thresholds (0.1 step size from 0.2 to 2.6). The

721 preferred P/S ratio cutoff is 1.2 at 10-18Hz (AUC=0.98), which leads to a true positive rate of

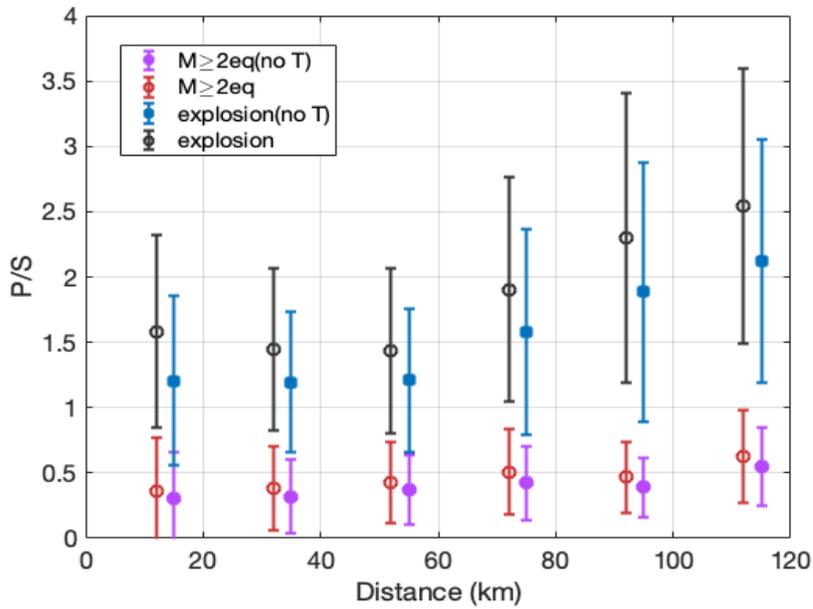
722 100% and false positive rate of 4.93%. C&D) Similar to A&B) but showing bootstrapping results

723 using only  $M_L \geq 2$  earthquakes. The bold lines are averaged curves from 1000 subsets and the

724 three dots mark the highest AUC. Note that a few outliers exhibit near-random performance for

725 the 4-station case (light blue near the diagonal in C) and a few others may reach AUC=1 while

726 the averages (bold curves) are below 1 for 4-station and 16-station cases (in D).



727

728 Figure 12. Effect of transverse component P-wave energy on P/S ratios. The error bars show  
 729 medians and SMAD values of 10-18 Hz P/S ratios in 20 km bins for all source-station pairs  
 730 (similar to Figure 6a but using only  $M_L \geq 2$  earthquakes and all explosions).

731