

1 **Caldera Collapse Geometry Revealed by Near-field GPS**  
2 **Displacements at Kīlauea Volcano in 2018**

3 **Paul Segall<sup>1</sup>, Kyle R. Anderson<sup>2</sup>, Fabio Pulvirenti<sup>3</sup>, Taiyi Wang<sup>1</sup>, Ingrid**  
4 **Johanson<sup>4</sup>**

5 <sup>1</sup>Geophysics, Stanford University

6 <sup>2</sup>U.S. Geological Survey, California Volcano Observatory

7 <sup>3</sup>Jet Propulsion Laboratory, Caltech

8 <sup>4</sup>U.S. Geological Survey, Hawaiian Volcano Observatory

9 **Key Points:**

- 10 • Discrete collapse events exhibit radial outward displacements up to 20 cm and up-  
11 lift of over 5 cm outside caldera
- 12 • Data best fit by slip on normal ring-fault that steepens with depth and associated  
13 pressurization of underlying magma chamber
- 14 • Triaxial point source fits the data well, but yields a strongly biased estimate of  
15 the source depth and kinematics

## Abstract

We employ near-field GPS data to determine the subsurface geometry of a collapsing caldera during the 2018 Kilauea eruption. Collapse occurred in 62 discrete events, with “inflationary” deformation external to the collapse, similar to previous basaltic collapses. We take advantage of GPS data from the collapsing block, and independent constraints on the magma chamber geometry from inversion of deflation prior to collapse onset. This provides an unparalleled opportunity to constrain the collapse geometry. Employing an axi-symmetric finite element model, the co-collapse displacements are best explained by piston-like subsidence along a high angle ( $\sim 85^\circ$ ) normal ring-fault that may steepen to vertical with depth. Reservoir magma has compressibility of  $2 \rightarrow 15 \times 10^{-10} \text{ Pa}^{-1}$ , indicating bubble volume fractions from 1 to 7 % (lower if fault steepens with depth). Magma pressure increases during collapses are 1 to 3 MPa, depending on compressibility. A tri-axial point source in a homogeneous half-space fits the data well, but provides a biased representation of the source depth and process.

## Plain Language Summary

When large volumes of magma erupt rapidly the rock overlying the subsurface reservoir founders producing a caldera. During the 2018 eruption of Kilauea volcano, Hawaii collapse occurred in over 60 events, each lasting 5 to 10 seconds. We analyze GPS data collected during the last 32 of these events to determine the geometry of the ring fault system bounding the caldera block and the properties of the underlying magma. The faults are on average very steep, but slightly inward dipping at shallow depth. Inferred pressure increases during collapse events constrain the compressibility of the magma and imply an exsolved gas phase with from 1 to 7 % bubbles by volume.

## 1 Introduction

The largest volcanic eruptions are accompanied by caldera collapse. While caldera formation is understood to result from the rapid withdrawal of large volumes of magmas from crustal reservoirs, the geometry of these reservoirs and in particular the dip of the ring-fault systems (normal vs reverse) are not well understood. Constraints come from geologic observations of eroded calderas, geophysical observations, as well as analog and numerical modeling (*Cole et al.*, 2005; *Branney and Acocella*, 2015). Caldera col-

46 lapses are thankfully rare and relatively little data has been collected in the near field  
47 of an ongoing collapse.

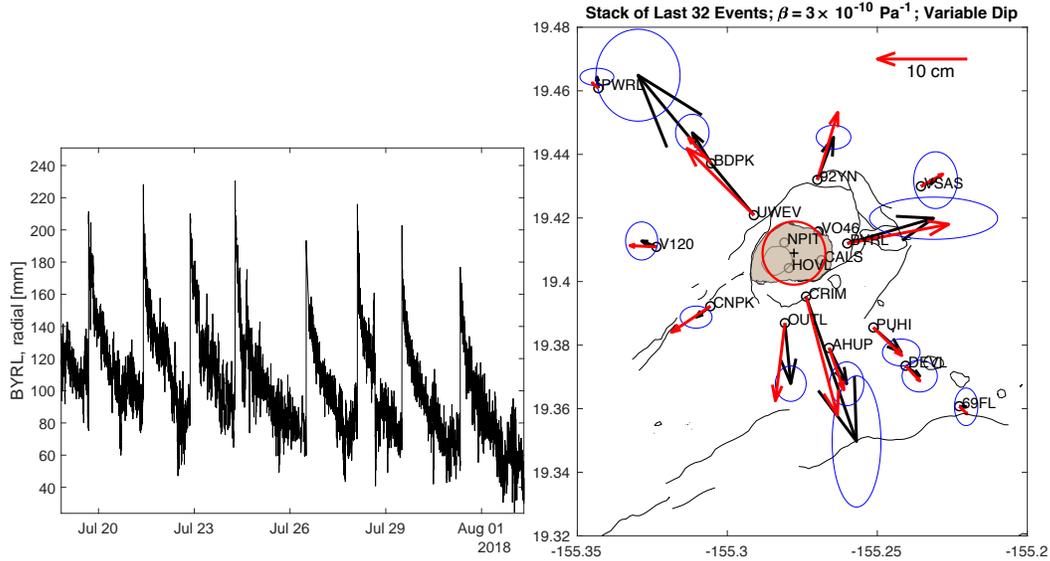
48 Historic caldera collapses at basaltic shield volcanoes occur in discrete events; the  
49 Kīlauea 2018 eruption consisted of 62 such collapse events (*Neal et al., 2019; Tepp et al.,*  
50 2020). These events were accompanied by very long period (VLP) earthquakes and re-  
51 markable “inflationary” deformation (Figure 1). Similar behavior was observed at Miyake-  
52 jima, Japan and Piton de la Fournaise on Reunion Island (*Kumagai et al., 2001; Michon*  
53 *et al., 2009*). Kīlauea high rate GPS data show that the collapse events took place over  
54 5 to 10 seconds. During this time negligible magma could have left the underlying cham-  
55 ber, meaning that collapses occurred under constant mass conditions. *Segall et al. (2019)*  
56 showed that under these conditions co-collapse deformation results from a combination  
57 of chamber pressurization and fault slip. For a vertical ring-fault the deformation exter-  
58 nal to the collapse is caused solely by pressure increase in the chamber; for other dips  
59 fault-induced deformation contributes to surface displacements and tilts.

60 The eruption of Kīlauea in 2018 provided unique data during a caldera collapse (*Neal*  
61 *et al., 2019; Anderson et al., 2019; Tepp et al., 2020*). The eruption began on May 3, 2018  
62 in the lower East Rift Zone (ERZ). Deflation at Kīlauea’s summit began the previous  
63 day and accelerated following a M 6.9 south flank earthquake on May 4. On May 16 the  
64 first rapid inflation event occurred contemporaneous with significant ash emission. By  
65 May 29 fault-bounded collapse was evident outside of Halema’uma’u crater. Later in the  
66 eruption collapse events were accompanied by higher effusion rates at the eruption site  
67 (*Patrick et al., 2019*). During June a new surface fault scarp propagated clockwise through  
68 the existing (1500 CE) Kīlauea caldera, establishing a roughly circular collapse struc-  
69 ture by mid to late June 2018. The floor of Halema’uma’u crater ultimately dropped up  
70 to 500 meters and the volume of the caldera increased by  $\sim 0.8 \text{ km}^3$ .

71 Here we build on the conceptual modeling of *Segall et al. (2019)*; specifically, we  
72 use near-field GPS data to constrain collapse structure at depth. We develop a forward  
73 model conditioned on observations prior to collapse onset. Unknown parameters are con-  
74 strained by near-field, co-collapse GPS displacements. To contrast with point source mod-  
75 els commonly employed in volcano deformation studies, we compare results with inver-  
76 sions based on a tri-axial point source in a homogeneous half-space. The point source  
77 has more degrees of freedom than the finite element method (FEM) based model, and

78 is not restricted to radial symmetry. Nevertheless, it cannot capture the kinematics of  
 79 the collapse and could lead to biased interpretations.

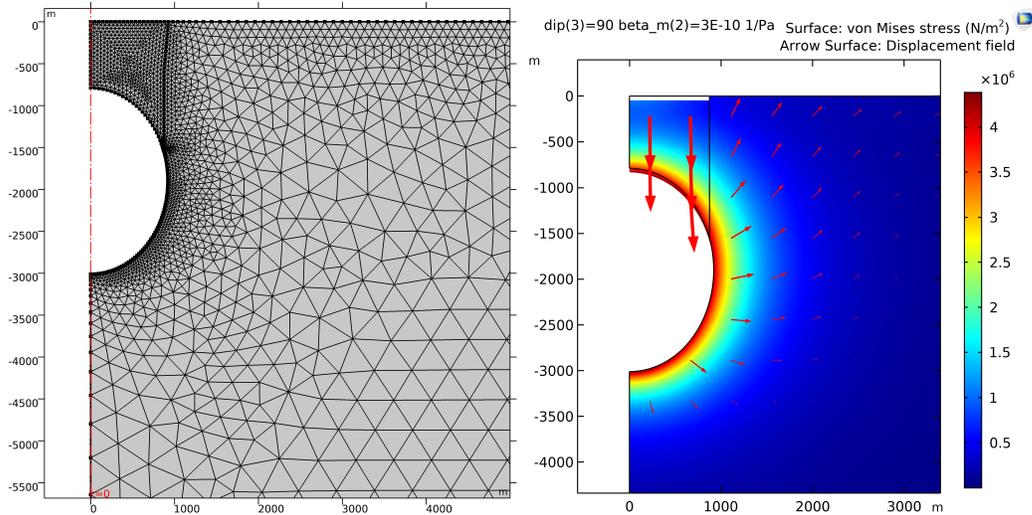
80 **2 Method**



**Figure 1.** A) Time series of radial component GPS displacements at BYRL. Positive displacement indicates motion away from the caldera. Station location shown in B. B) Co-collapse radial displacements. Black: average of last 32 collapse events, with 95% confidence ellipses reflecting the variability of the individual events. Red: predicted by model with fault dip increasing from  $85^\circ$  to vertical at 600 m (see Figure 2) and magma compressibility  $\beta_m = 3 \times 10^{-10} \text{ Pa}^{-1}$ . Collapse structure is shaded. Red circle shows location of model ring-fault. Scale vector is 0.1 m.

81 We analyze high rate GPS data (5 second sampling) from collapse events later in  
 82 the eruption, after the eastern section of the ring-fault system was fully formed. A sam-  
 83 ple time series for station BYRL is shown in Figure 1a. The co-collapse displacement  
 84 in individual events was determined as the difference between pre- and post event po-  
 85 sitions averaged over 5 minutes, not including a window  $\pm 1$  minute around the time of  
 86 the event. We then computed the mean and variance of the co-collapse displacements  
 87 for the last 32 events. We find that stations closest to the collapse have more variabil-  
 88 ity and are thus down-weighted relative to more distant stations in our inversions. An  
 89 alternate approach is to stack time series at each station (last 32 events), and then com-  
 90 pute co-collapse displacements from the stack. Uncertainties in this case are computed

91 by taking the standard deviation of samples in the 4-minute pre- and post-collapse win-  
 92 dows and propagating these uncertainties into the offset, assuming they are uncorrelated  
 93 and normally distributed. While these two approaches lead to essentially identical dis-  
 94 placements stacking results in substantially smaller but more uniform uncertainties. For  
 95 completeness we present results with both sets of weights.



**Figure 2.** A) Finite element mesh showing the magma chamber and an inward dipping fault that steepens with depth. Geometry is radially symmetric about the red dashed line. B) Maximum shear (von Mises) stress for vertical ring-fault. Vectors represent displacements with log scaling to permit viewing of displacements outside the collapse piston. Note that stresses are due solely to chamber pressurization.

96 We take advantage of constraints on the magma chamber geometry inferred from  
 97 analysis of pre-collapse deflation measured by GPS, tilt, and InSAR (*Anderson et al.*,  
 98 2019). We take the median values for the chamber parameters to construct a radially  
 99 symmetric FEM model of a typical collapse event (Figure 2). The model consists of an  
 100 ellipsoidal reservoir and a ring-fault from the surface to the magma chamber. Of course,  
 101 neither the collapse geometry nor displacements are radially symmetric (Figure 1b). Rather,  
 102 the collapse occurred on pre-existing faults along much of the south and west margins,  
 103 whereas a new (at least at the surface) intra-caldera fault developed along the east mar-  
 104 gin of the 2018 collapse. High frequency (volcano tectonic, VT) seismicity was concen-  
 105 tred along this new structure (*Shelly and Thelen, 2019*).

106 From *Anderson et al.* (2019) (see Supplemental Information) the median magma  
 107 chamber has initial volume  $V = 3.9 \text{ km}^3$ , and centroid depth 1.9 km, whose apex reaches  
 108 to  $\sim 0.8 \text{ km}$  below the surface (Figure 2). Note that the pre-collapse model places only  
 109 first-order constraints on the shape of and depth to the top of the reservoir. The aver-  
 110 age vertical displacement during the last 32 collapse events, from GPS station CALS lo-  
 111 cated on the down-dropped block (Figure 1b) was  $\sim 2.5$  meters. Thus, fault slip, as-  
 112 sumed for simplicity to be uniform along the ring-fault, is taken as  $2.5/\sin(\delta)$  meters,  
 113 where  $\delta$  is fault dip.

114 The surface deformation during collapse events depends on the geometry of the magma  
 115 chamber and ring-fault system, and the pressure change induced by reduction in cham-  
 116 ber volume due to downward motion of the roof block. As shown in Supplemental In-  
 117 formation, the co-collapse displacements  $u_{\text{co}}(\mathbf{x})$  at radial position  $\mathbf{x}$  are

$$u_{\text{co}}(\mathbf{x}) = s \left[ \frac{-\Phi(\mathbf{m}, \delta)f(\mathbf{x}; \mathbf{m})}{\mu(\beta_m + \beta_c)} + g(\mathbf{x}; \mathbf{m}, \delta) \right]. \quad (1)$$

118 Here  $s$  is fault slip,  $f(\mathbf{x}; \mathbf{m})$  is function of model parameters  $\mathbf{m}$  that characterize the cham-  
 119 ber ( depth to centroid, vertical and horizontal semi-axes);  $g(\mathbf{x}; \mathbf{m}, \delta)$  is a dimensionless  
 120 function that maps slip to displacement at constant chamber pressure. Further,  $\Phi \equiv$   
 121  $\partial V/\partial s$  at constant  $p$ . Finally,  $\mu$  is the crustal shear modulus,  $\beta_m$  and  $\beta_c \equiv (1/V)\partial V/\partial p$   
 122 are the magma and chamber compressibilities. The latter depends on  $\mu$  and chamber ge-  
 123 ometry. Note  $\Phi f$  and  $\mu(\beta_m + \beta_c)$  are dimensionless.

124 The average elastic properties of the crust are imperfectly known, but are chosen  
 125 to be consistent with the pre-collapse modeling. The surface expression of the ring-fault  
 126 is constrained by direct observation and roughly coincides with the inferred outline of  
 127 the magma chamber (*Anderson et al.*, 2019). By fixing the geometry (including  $V$ ) and  
 128  $\mu$ , which determines both  $\beta_c$  and  $\Phi$  to that estimated from pre-collapse data, the only  
 129 unknown parameters are fault dip and magma compressibility. We search over  $(\delta, \beta_m)$   
 130 space to determine parameters that optimize fit to the co-collapse data.

Equation (1) is important for understanding how the data scale with mechanical  
 and geometric parameters. As described in the SI, the pressure change in the first term  
 does not appear explicitly. However, in the FEM calculations  $\Delta p_{\text{co}}$  induced by collapse

is computed by

$$\Delta p_{\text{co}} = -\frac{\Delta V}{V\beta_m}, \quad (2)$$

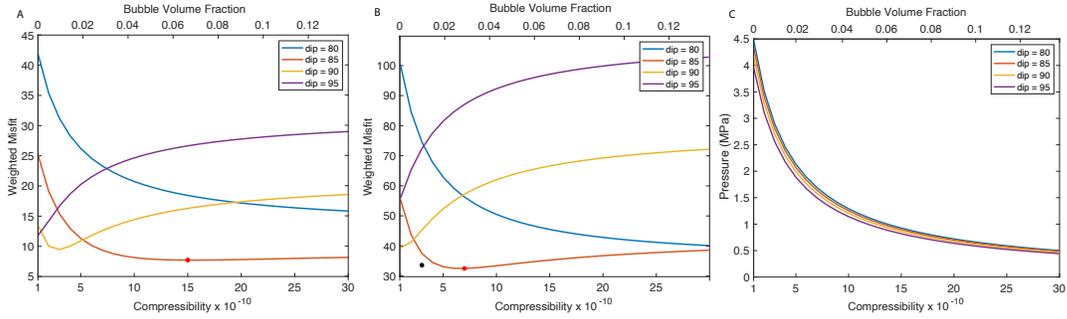
131 where  $\Delta V$  is the change in chamber volume.

132 We use the finite element code COMSOL Multiphysics to determine the surface  
 133 deformation due to fault slip on a ring-fault coupled to a magma chamber (Figure 2).  
 134 Slip is spatially uniform and imposed on the ring-fault. Displacement of the plug into  
 135 the chamber reduces its volume, increasing magma pressure according to equation (2).  
 136 This spatially uniform pressure change and zero shear traction provide the boundary con-  
 137 dition on the walls of the chamber. The model domain dimensions are 20x the largest  
 138 dimension of the chamber, sufficient to avoid boundary effects; results are insensitive to  
 139 mesh refinement. We search over a range of fault dips and magma compressibilities and  
 140 compare to the observed displacements.

### 141 3 Results

142 Figure 3 shows misfit, defined as the weighted residual 2-norm, including vertical  
 143 and radial displacements, as a function of dip and compressibility. Figure 3a shows re-  
 144 sults with weights determined by the variance of the events, while Figure 3b employs the  
 145 lower variance determined by first stacking the last 32 events. In both cases it is clear  
 146 that a (normal) dip of  $85^\circ$  fits the data best over a range of compressibilities, with op-  
 147 timal values of  $\beta_m$  of 15 and  $7 \times 10^{-10} \text{ Pa}^{-1}$ , respectively. Vertical ring-faults with  $\beta_m =$   
 148  $1 \rightarrow 3 \times 10^{-10} \text{ Pa}^{-1}$  also fit the data with larger errors reasonably well (Fig. 3a). Shal-  
 149 lower normal faults ( $\delta \leq 85^\circ$ ) and reverse faults ( $\delta = 95^\circ$ ) generally do not fit the data  
 150 well.

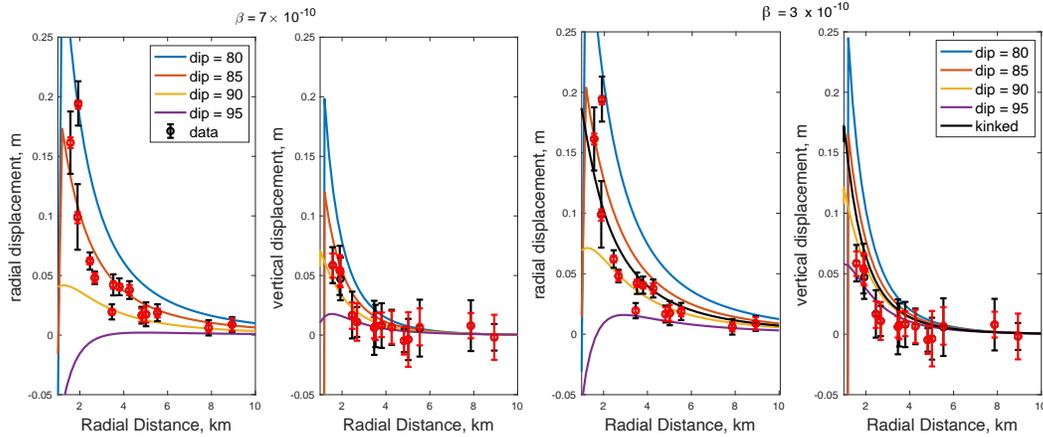
151 Figure 4a,b compare radial and vertical displacements as a function of distance from  
 152 the collapse center with predictions from the FEM model for the optimal magma com-  
 153 pressibility,  $\beta_m = 7 \times 10^{-10} \text{ Pa}^{-1}$ , and a range of ring-fault dips. The  $85^\circ$  dipping ring-  
 154 fault fits data quite well, although under-predicting the radial displacements of the near-  
 155 est stations (CRIM and UWEV). As noted by *Segall et al.* (2019), outward dips ( $> 90^\circ$ )  
 156 result in inward directed (negative) displacements close to the collapse, contrary to ob-  
 157 servations. This is most pronounced with compressible magmas because of the smaller  
 158 pressure change (Figure 3c), which increases the relative contribution of the ring-fault  
 159 to the surface deformation. With less compressible magmas (see SI) the predicted ra-



**Figure 3.** Weighted residual norm as a function of fault dip and magma compressibility. Red star indicates minimum misfit. Top axis gives the implied bubble volume fraction (see Discussion). a) Standard deviation determined from the 32 separate events. b) Standard deviation determined from stack of events. Black star indicates misfit for fault with variable dip. c) Computed pressure change in the magma chamber.

160 dial displacements are outward, but decrease as the ring-fault is approached, contrary  
 161 to the data (SI Fig. 1). These observations exclude an outward dipping ring-fault. With  
 162 the compressibility of gas free basalt, the minimum reasonable value,  $\beta_m \sim 1 \times 10^{-10} \text{ Pa}^{-1}$ ,  
 163 the model over predicts the vertical displacements for all dips (SI). As described in the  
 164 Discussion, these results imply the presence of an exsolved vapor phase in the magma  
 165 chamber.

166 Figure 4c,d illustrates results for  $\beta_m = 3 \times 10^{-10} \text{ Pa}^{-1}$ , near the local minimum  
 167 in misfit for a vertical ring-fault (Fig. 3a). For this compressibility, the vertical ring-fault  
 168 fits the radial displacements well at more distant stations (Fig. 4c), but significantly under-  
 169 predicts the radial displacements at the closer stations. While the  $85^\circ$  dipping fault bet-  
 170 ter fits the close-in radial displacements, it over predicts both the more distant stations  
 171 as well as the vertical displacements. This suggests that the ring-fault may steepen with  
 172 depth, which we tested for a number of scenarios. Figure 4c,d shows the prediction for  
 173 a ring-fault that dips  $85^\circ$  at the surface and steepens to vertical at 600 m depth (Fig.  
 174 2a). As expected, this fits the radial displacements at the more distant stations and does  
 175 a better job of fitting the closer stations. It over predicts the vertical displacements, but  
 176 generally fits the data within one standard deviation. Dips that steepen with depth are  
 177 consistent with field observations that show inward (normal) dips at the surface. (The  
 178 ratio of vertical to horizontal displacements at CALS (see Fig. 1b) indicate a dip at the  
 179 earth's surface of  $71.5^\circ$ ).



**Figure 4.** Predicted and observed radial (a,c) and vertical (b,d) displacements during a collapse event. 1-sigma error bars; simple averaging (black) and stacking (red). Predictions are shown for a range of dips (dips less than  $90^\circ$  are normal faults) and  $\beta_m = 7 \times 10^{-10} \text{ Pa}^{-1}$  (a,b) and for  $\beta_m = 3 \times 10^{-10} \text{ Pa}^{-1}$  (c,d). Also shown is the case with fault dip that steepens from  $85^\circ$  to vertical at a depth of 600m, labeled “kinked”.

180 The fit to the horizontal displacements of the steepening fault model is shown in  
 181 Figure 1b. The model under predicts the displacement at UWEV and over predicts the  
 182 displacements at CNPK and 92YN, a consequence of the assumed radial symmetry. Some  
 183 aspect of the ring-fault chamber system led to larger displacements in the northwestern  
 184 direction at UWEV, although BDPK is fit well, suggesting this feature is shallow. One  
 185 possibility is a locally shallower dip along this section of the ring-fault. It is also pos-  
 186 sible that there is some asymmetry in the shallow magma reservoir, although asymme-  
 187 try in the pre-collapse deformation was small (*Anderson et al.*, 2019). Given the sym-  
 188 metry of the forward model and the fact that only two parameters are adjusted, the fit  
 189 is reasonable.

190 The pressure increase during a typical collapse event is shown in Figure 3c. Because  
 191 the slip amplitude is specified, less compressible magmas result in larger pressure increases  
 192 (equation 2). Fault dip has a minor effect with normal faulting giving slightly larger pres-  
 193 sure increases. Given the range of parameters that fit the data, our results suggest that  
 194 pressure increases ranged from 3.3 MPa (for a vertical ring-fault and a compressibility  
 195 of  $2 \times 10^{-10} \text{ Pa}^{-1}$ ) to 1.25 MPa (for an  $85^\circ$  dip and compressibility of  $10^{-9} \text{ Pa}^{-1}$ .)

## 4 Discussion

The compressibility of gas-free basalt is  $\beta_l \sim 1 \times 10^{-10} \text{ Pa}^{-1}$  (Murase and McBirney, 1973; Spera, 2000). Our results suggest the compressibility of magma in the Halema'uma'u reservoir is  $\beta_m = 2 \rightarrow 15 \times 10^{-10} \text{ Pa}^{-1}$ , implying an exsolved gas phase. The magma compressibility can be expressed in terms of the volume fraction of gas phase  $\phi$ ,

$$\beta_m = (1 - \phi)\beta_l + \phi\beta_g = (1 - \phi)\beta_l + \phi/p, \quad (3)$$

where the gas is assumed to be ideal. Taking the pressure to be magmastatic at the chamber centroid depth, with density  $2.5 \times 10^3$  implies vesicularities of  $\phi$  of 0.01 to 0.07, and possibly as high as 0.12 (Fig. 3). Given that bubbles rise rapidly in low viscosity basalt, high *in situ* gas volume fractions may be unrealistic, however it is beyond our scope to bound plausible values. It also should be noted from equation (1) that displacements depend on the product of shear modulus  $\mu$  and total compressibility. It is possible that the effective shear modulus for short-duration collapse events may have been greater than that for weeks-long deflation. If so, this could be consistent with lower compressibility and vesicularity.

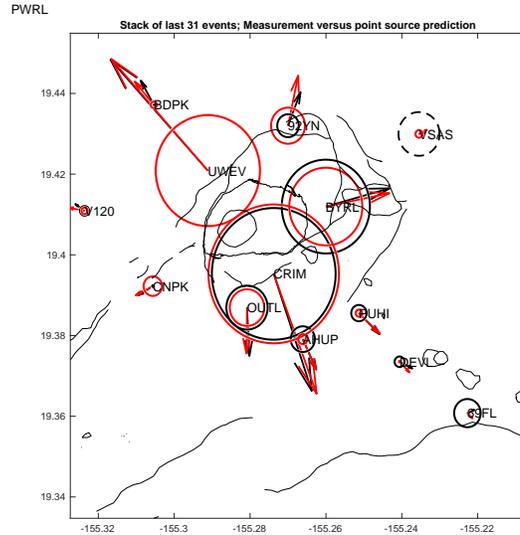
We used the  $\sim 2.5$  m rapid downward displacement of CALS (Figure 1b) to measure sudden collapse in a typical event. CALS also experienced  $\sim 2$  m slow subsidence between collapse events. This may reflect fault creep, perhaps localized along the newer, eastern sector of the ring-fault associated with abundant VT seismicity (Shelly and Thelen, 2019). Because CALS is close to the eastern ring-fault, it is possible that it is unrepresentative of the collapse as a whole. If the main collapse experienced the cumulative displacement at CALS it would have been closer to 4.5 meters.

The cumulative displacements recorded from repeated digital elevation models (DEM) provide another estimate of the vertical drop in an average collapse. Between July 13 and the end of the eruption the eastern block subsided about 60-70 m, in 13 events, or  $\sim 5$  meters per event. However, this does not determine how much was slow inter-event subsidence. We find that solutions with 5 meters of slip do not fit as well, especially at the closest stations, and favor vertical ring-faults. Because the slow inter-event displacement at CALS coincides with VT seismicity, we favor the interpretation that vertical displacement per event is closer to 2.5 m, but with only one site on the down-dropped block we cannot rule out up to 5 m of collapse.

226 Our calculations have not accounted for the Overlook vent, or topographic effects  
 227 of the pre-existing (1500 CE) caldera or newly formed collapse pit as it was expressed  
 228 in mid June, 2018 at the start of the data analyzed here. Forward models including a  
 229 conical “pit” with radius 700 m and depth up to 300 m did not significantly alter the con-  
 230 clusions presented here. The pit has greatest effect on horizontal displacements, partic-  
 231 ularly with the reverse ring-fault geometry. Deeper pits and significant disk-shaped calderas  
 232 have more significant effects. Full three dimensional modeling with accurate surface to-  
 233 pography is beyond our scope, but appears unlikely to fundamentally alter our conclu-  
 234 sions.

235 The results above fix the magma chamber geometry to the median values deter-  
 236 mined from analysis of pre-collapse deflation. To explore the effects of uncertainty in cham-  
 237 ber geometry on inferred properties, we resample from the posterior distribution of *An-*  
 238 *derson et al.* (2019). For a vertical ring-fault the surface deformation outside the collapse  
 239 is simply rigid body translation of the piston plus pressurization of the chamber (*Segall*  
 240 *et al.*, 2019) (see also below). Thus, we can employ the model emulator developed by *An-*  
 241 *derson et al.* (2019) to predict the surface deformation due to a co-collapse pressure in-  
 242 crease. Least squares estimation of pressure change  $\Delta p_{co}$  given by equation (2), assum-  
 243 ing 2.5 m subsidence per event, along with other parameters are shown in the Supple-  
 244 mental Information (SI Fig. 2).  $\Delta p_{co}$  is normally distributed with a mean of 3 MPa and  
 245 standard deviation of 0.3 MPa. The inferred magma compressibility ranges from roughly  
 246  $3 \times 10^{-10}$  to  $2 \times 10^{-9}$  Pa<sup>-1</sup>. While this range is for vertical ring-faults it may reason-  
 247 ably approximate normal faults that steepen to vertical at shallow depth.

248 Volcano deformation studies often model source processes with point source approx-  
 249 imations of magma chambers. To contrast this with the finite source model above, we  
 250 invert the co-collapse displacements for a tri-axial point-source. A single point source  
 251 necessarily combines the contributions of the ring-fault and the magma chamber in a sin-  
 252 gle source, although the true source is distributed in depth. We follow the procedure of  
 253 *Davis* (1986) see also *Segall* (2010, Chapter 7), using Green’s tensors for a homogeneous  
 254 half-space, but do not associate the double forces in terms of a pressure boundary con-  
 255 dition on a spheroidal magma chamber. We restrict one double force to vertical; relax-  
 256 ing this improves the fit somewhat, but does not alter the interpretation. We estimate  
 257 the source location and the best-fitting moment tensor with a Markov Chain Monte Carlo  
 258 (MCMC) procedure.



**Figure 5.** Comparison of observed co-collapse displacements (black) with those predicted by a generalized point-source moment tensor in an elastic half-space (red). Circles represent vertical displacements, dashed where negative.

259 The point source model fits the data quite well (Figure 5). Posterior distributions  
 260 for the point-source parameters are given in the SI (SI Fig. 3). The median source depth  
 261 is  $\sim 700$  m, much shallower than the chamber centroid inferred from pre-collapse data  
 262 (*Anderson et al.*, 2019). While the point source combines contributions from the ring-  
 263 fault and magma chamber, which are at different depths, it should be dominated by the  
 264 chamber for near vertical ring-faults. Thus, the source depth is unrealistically shallow.  
 265 The best fitting source is largely isotropic expansion (SI Fig. 4) with minor CLVD and  
 266 double couple components. The vertical double-force is maximum; the largest horizon-  
 267 tal double-force is directed NW/SE reflecting the displacements at UWEV and CRIM  
 268 (Figure 9b) compared to the orthogonal NE/SW direction.

269 An expansion source might seem counterintuitive for a collapsing caldera, because  
 270 the “inflationary” deformation observed outside the collapse structure is caused by a vol-  
 271 ume *decrease* but a pressure *increase*. Consider the case of a vertical ring-fault: Due to  
 272 linearity in the problem the forward model can be decomposed into: 1) displacement of  
 273 the piston into a magma chamber at constant pressure, and 2) the pressurization of the  
 274 chamber due to the resulting volume decrease. The first step is a rigid body motion and  
 275 produces no deformation outside the piston. Thus, for a vertical ring-fault the pressure  
 276 increase is the sole cause of deformation external to the caldera. This indicates that there

277 should be some caution in interpreting moment tensor estimates for volumetric sources  
 278 in terms of source kinematics. We also explored forcing the point source to be located  
 279 at the *a priori* chamber centroid depth. Not surprisingly, fit to the co-collapse displace-  
 280 ments is degraded; in particular, the vertical displacements are significantly over-predicted.

281 As noted above, the collapse faults are normal at the surface, while the geodetic  
 282 data are consistent with dips steepening with depth. In contrast, many analog and nu-  
 283 merical models (*Acocella, 2007; Ruch et al., 2012; Holohan et al., 2011; Geyer and Martí,*  
 284 *2014*) find initial development of an inner reverse ring-fault with subsequent growth of  
 285 a peripheral fault that may have a normal geometry. In contrast to these studies, the  
 286 Kīlauea collapse was clearly influenced by the presence of the lava lake, Halema’uma’u  
 287 crater, and pre-existing caldera bounding structures. In particular, the presence of the  
 288 lava lake conduit seems to have promoted inward slumping. Another factor favoring nor-  
 289 mal faulting is regional extension (*Acocella, 2007*), which is present at Kīlauea due to  
 290 seaward motion of the volcano’s south flank (*Owen et al., 2000; Denlinger and Morgan,*  
 291 *2014*).

## 292 5 Conclusions

- 293 • Collapse events were accompanied by remarkable “inflationary” deformation ex-  
 294 ternal to the caldera with radial outward displacements of nearly 20 cm and up-  
 295 lift of over 5 cm.
- 296 • For a constant fault dip the data are best fit by a steeply dipping ( $85^\circ$ ) normal  
 297 ring-fault with a magma estimated to have on the order of 3% bubble volume frac-  
 298 tion.
- 299 • For lower bubble volume fractions, fit to the stations closest to the caldera is im-  
 300 proved if the fault dip increases from roughly  $85^\circ$  to vertical at a depth of  $\sim 600$   
 301 meters, qualitatively consistent with normal faulting observed at the surface.
- 302 • Estimates of pressure increases during collapse events range from 1 to over 3 MPa,  
 303 depending on magma compressibility. Uncertainty in magma chamber volume alone  
 304 introduces an uncertainty in pressure change on the order of 0.3 MPa.
- 305 • A generalized triaxial point source can fit the data quite well, but yields a strongly  
 306 biased estimate of the source depth and kinematics.

307 **Acknowledgments**

308 Thanks to Gary Mavko for discussion. GPS data are available from the UNAVCO archive:

309 <https://www.unavco.org/data/data.html>

310 **References**

- 311 Acocella, V. (2007), Understanding caldera structure and development: An overview  
 312 of analogue models compared to natural calderas, *Earth-Science Reviews*, *85*(3-4),  
 313 125–160.
- 314 Anderson, K. R., I. A. Johanson, M. R. Patrick, M. Gu, P. Segall, M. P. Poland,  
 315 E. K. Montgomery-Brown, and A. Miklius (2019), Magma reservoir failure and the  
 316 onset of caldera collapse at kīlauea volcano in 2018, *Science*, *366*(6470).
- 317 Branney, A., and V. Acocella (2015), Calderas, in *The encyclopedia of volcanoes*,  
 318 edited by H. Sigurdsson, pp. 299–315, Elsevier.
- 319 Cole, J., D. Milner, and K. Spinks (2005), Calderas and caldera structures: a review,  
 320 *Earth-Science Reviews*, *69*(1-2), 1–26.
- 321 Davis, P. M. (1986), Surface deformation due to inflation of an arbitrarily oriented  
 322 triaxial ellipsoidal cavity in an elastic half-space, with reference to kilauea volcano,  
 323 hawaii, *Journal of Geophysical Research: Solid Earth*, *91*(B7), 7429–7438.
- 324 Denlinger, R. P., and J. K. Morgan (2014), Instability of Hawaiian volcanoes, *Char-*  
 325 *acteristics of Hawaiian volcanoes, 1801*, 149–176.
- 326 Geyer, A., and J. Martí (2014), A short review of our current understanding of the  
 327 development of ring faults during collapse caldera formation, *Frontiers in Earth*  
 328 *Science*, *2*, 22.
- 329 Holohan, E., M. Schöpfer, and J. Walsh (2011), Mechanical and geometric controls  
 330 on the structural evolution of pit crater and caldera subsidence, *Journal of Geo-*  
 331 *physical Research: Solid Earth*, *116*(B7).
- 332 Kumagai, H., T. Ohminato, M. Nakano, M. Ooi, A. Kubo, H. Inoue, and J. Oikawa  
 333 (2001), Very-long-period seismic signals and caldera formation at Miyake island,  
 334 Japan, *Science*, *293*(5530), 687–690.
- 335 Michon, L., N. Villeneuve, T. Catry, and O. Merle (2009), How summit calderas  
 336 collapse on basaltic volcanoes: New insights from the april 2007 caldera collapse of  
 337 Piton de la Fournaise volcano, *Journal of Volcanology and Geothermal Research*,  
 338 *184*(1-2), 138–151.
- 339 Murase, T., and A. R. McBirney (1973), Properties of some common igneous rocks  
 340 and their melts at high temperatures, *Geological Society of America Bulletin*,  
 341 *84*(11), 3563–3592.

- 342 Neal, C., S. Brantley, L. Antolik, J. Babb, M. Burgess, K. Calles, M. Cappos,  
 343 J. Chang, S. Conway, L. Desmither, et al. (2019), The 2018 rift eruption and  
 344 summit collapse of Kīlauea volcano, *Science*, *363*(6425), 367–374.
- 345 Owen, S., P. Segall, M. Lisowski, A. Miklius, R. Denlinger, and M. Sako (2000),  
 346 Rapid deformation of Kilauea volcano: Global positioning system measurements  
 347 between 1990 and 1996, *J. Geophys. Res.*, *105*(B8), 18,983 – 18,998.
- 348 Patrick, M., H. Dietterich, J. Lyons, A. Diefenbach, C. Parcheta, K. Anderson,  
 349 A. Namiki, I. Sumita, B. Shiro, and J. Kauahikaua (2019), Cyclic lava effusion  
 350 during the 2018 eruption of kīlauea volcano, *Science*, *366*(6470).
- 351 Ruch, J., V. Acocella, N. Geshi, A. Nobile, and F. Corbi (2012), Kinematic analysis  
 352 of vertical collapse on volcanoes using experimental models time series, *Journal of*  
 353 *Geophysical Research: Solid Earth*, *117*(B7).
- 354 Segall, P. (2010), *Earthquake and Volcano Deformation*, 432 pp., Princeton Univ.  
 355 Press.
- 356 Segall, P., K. R. Anderson, I. Johanson, and A. Miklius (2019), Mechanics of infla-  
 357 tionary deformation during caldera collapse: Evidence from the 2018 kī lauea  
 358 eruption, *Geophysical Research Letters*.
- 359 Shelly, D. R., and W. A. Thelen (2019), Anatomy of a caldera collapse: Kīlauea  
 360 2018 summit seismicity sequence in high resolution, *Geophysical Research Letters*.
- 361 Shuler, A., G. Ekström, and M. Nettles (2013), Physical mechanisms for vertical-  
 362 clvd earthquakes at active volcanoes, *Journal of Geophysical Research: Solid*  
 363 *Earth*, *118*(4), 1569–1586.
- 364 Spera, F. (2000), Physical properties of magma, in *Encyclopedia of Volcanoes*, edited  
 365 by H. Sigurdsson, pp. 171–190, Academic Press, San Diego, CA, USA.
- 366 Tepp, G., A. Hotovec-Ellis, B. Shiro, I. Johanson, W. Thelen, and M. M. Haney  
 367 (2020), Seismic and geodetic progression of the 2018 summit caldera collapse of  
 368 kīlauea volcano, *Earth and Planetary Science Letters*, *540*, 116,250.