

Synthesis of Ricinoleate Anion based Ionic Liquids and their Application as Green Lubricating oil Additives

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Abstract

Ricinoleate anion based ionic liquids (ILs) were synthesized from four different nitrogen containing cationic counterparts such as tetrabutylammonium, tetrapropylammonium, cetyltrimethylammonium, imidazolium and evaluated for tribological performance in two lubricant base stocks. From the tribological tests it was found that the synthesized ILs in base oil significantly reduced the wear scar diameter by 17-25 % and a remarkable reduction in wear observed for all the tested load and rotation speed at optimized concentration and also improved the load carrying capacity by 25-43%. The results conclude that the cation present in IL control the thermal stability, antiwear and extreme pressure properties. The imidazolium cation containing IL showed the better performance among all the ILs being studied. Additionally, the morphology of worn surface and deposition of elementals on rubbed surface lubricated with base oil and base oil containing IL was studied by scanning electron microscope (SEM) and Energy-dispersive X-ray spectroscopy (EDX). The fatty acid constituted ILs are promising immense efficiency as environmentally friendly and renewable lubricant additives since they are free from halide, sulphate and phosphate ions.

Introduction

Ionic liquids (ILs) are molten salts containing organic or inorganic cations and anions which have lower boiling point than water (Battez et al., 2016; Khan et al., 2018; Khemchandani et al., 2014; Matczak et al., 2018). Their unique features such as high thermal stability, broad liquid range, low vapour pressure and non-flammability makes ionic liquids as versatile molecules for lubrication applications (Jimeenez and Bermudez, 2008; Pensado et al., 2008; Qu et al., 2006; Somers et al., 2013; Stolte et al., 2012; Yu et al., 2008). ILs offers some distinctive advantages in reducing friction and wear between surfaces in direct contact (Ichiro, 2009; Zhou et al., 2009). The ILs composed with ammonium, phosphonium, pyrrolidinium and imidazolium cations along with tetrafluoroborate, tosylate, halide and hexafluorophosphate anions were evaluated as lubricants and their interaction with metal surfaces was studied (Minami et al., 2010; Qu et al., 2006; Somers et al., 2012; Tiago et al., 2015; Zhou et al., 2009). These studies proved that the ILs act as neat lubricants and also as additives to the basestocks. It is believed that due to their inherent polarity ILs strongly adsorb on metal surfaces to form tribochemical film, this film enhances antiwear and antifriction performance (Liu et al., 2006; Mendonca et al., 2012; Mu et al., 2008; Qu et al., 2012; Ye et al., 2001). However, there is a limitation for using ILs as neat lubricants due to their higher cost and multistep reaction procedure involved in their synthesis compared to traditional base oils (Barnhill et al., 2014; Khan et al., 2018; Zhou et al., 2014). However, with a minimum weight percent of ILs in mineral oil and other synthetic oils performed better than the neat base oils (Amiril et al., 2017; Ma et al., 2019; Otero et al., 2014). Battez et al. detected the film forming capacity of phosphonium cation-based ILs at low concentrations in mineral oil and also evaluated the effect of IL concentration on film forming capacity and coefficient of friction under different test conditions. The choice of changing the combination of cation and anion is possible in ILs to attain specific properties (Ma et al., 2019; Mordukhovich et al., 2013; Salih et al., 2011). Recently some of

the ILs gained much interest as lubricant additives such as dicationic bis(ammonium) and bis(imidazolium)-di[bis(salicylato)borate] ionic liquids (Gusain et al., 2014), phosphonium-alkylphosphate (Qu et al., 2015) and N,N'-dialkylimidazolium (Pejakovic et al., 2016) etc. These ILs when used as additives to lubricating oil remarkably enhanced its antiwear and antifriction properties. Zhang et al. (2017), studied the synergistic effect of polymeric IL additives with conventional additive ZDDP and found best synergism with 1:1 w/w of ZDDP and boron-containing polyisobutylene-based IL. Compared to ZDDP ILs are ash less and have stronger adsorption towards metallic surface, thus they provide better lubricity performance with low engine deposits (Mendonca et al., 2012; Oulego et al., 2018).

Currently, most of the ionic liquid based additives used for the tribological applications were synthesized with anions such as the halide [F-, Cl-, Br- or I-], phosphate and sulfate these ILs exhaust high amount of toxic components to the environment. The ILs consisting of [PF₆]- and [BF₄]- shows severe corrosion effect due to the formation of hydrofluoric acid by vigorous reaction with water (Stolte et al., 2012; Swatloski et al., 2003). Kronberger et al. (2012), investigated the eco toxicity and bio degradability of lubricant additives with pyrrolidinium and quaternary ammonium based cations combined with CH₃O₄S-, CH₃O₃S- and (CF₃SO₂)₂N- as counter ions. The anion (CF₃SO₂)₂N- being highly resistant to biodegradation and cannot be considered for applications with potentially high environmental exposure. Conventional IL additives containing halide, sulphate and PF₆ anions are replaced with environmentally benign components like fatty acids and amino acids. Biodegradable and bio compatible behaviour of amino acid and fatty acid anions are alternatives to the hazardous anions. Liwen et al. synthesized two green ILs of choline with amino acids glycine and proline, these two ILs [choline][glycine] and [choline][L-proline] significantly improved the tribological properties of base oil (Mu et al., 2015). Minami et al. (2012), stated that the both tribological and thermo-oxidative stability depend on hydrophobicity of IL anion, as the hydrophobicity of anionic part increases results in improved performance. In recent years, the fatty acid derived ILs has been explored as environmentally benign lubricating oil additives. Khatri et al. (2018), reported the synthesis of tetramethylguanidinium ionic liquids with various fatty acid anions for steel/steel contact in grade I mineral oil. Long alkyl chain constituted ILs significantly reduced the friction and wear. The present work describes the synthesis of ricinoleate anion based ILs containing various cations and evaluation of their tribological performance by blending in base oil epoxy karanja 2-ethylhexyl esters (EKE) and dioctyl sebacate (DOS). The formation of tribofilms on surface with base oil and additive was investigated by SEM and EDX analysis was used to establish the elemental composition on the worn surfaces.

Experimental

Materials

Sodium ricinoleate was purchased from TCI chemicals (Tokyo, Japan), tetra butyl ammonium bromide (TBA-Br), tetra propyl ammonium bromide (TPA-Br), cetyl trimethyl ammonium bromide (CTA-Br) and butyl hexyl imidazolium bromide (BHI-Br) were purchased from Sigma Aldrich (St. Louis, USA). Highest grade purity of solvents were purchased from SD Fine Chemicals (Mumbai, India).

Characterization

The synthesized ionic liquids were characterized by ¹H and ¹³C NMR spectra on Varian 300 and 75 MHz, respectively using trimethylsilane (TMS) as internal standard. IR spectra were recorded on Perkin-Elmer Fourier transform (FT-IR) spectrum in chloroform solvent.

Synthetic Procedure

Ricinoleate anion-based ionic liquids having four variable nitrogen containing cations were synthesized by a facile metathesis reaction as per the earlier reported procedure (Gusain et al., 2016). The reaction proceeds in a single step by stirring equimolar ratio of both bromide salt and sodium ricinoleate in water for 18 h. The reaction mixture was extracted by using dichloromethane (DCM) followed by washing with distilled water to remove excess sodium ricinoleate and sodium bromide. The solvent was removed under reduced pressure and the obtained ionic liquids were dried for 48 h at 80 °C. The synthesized four ionic liquids tetra-

butylammonium (Z)-12-hydroxyoctadec-9-enoate (TBA-RA), tetrapropylammonium (Z)-12-hydroxyoctadec-9-enoate (TPA-RA), N,N,N-trimethylhexadecan-1-aminium (Z)-12-hydroxyoctadec-9-enoate (CTB-RA), 1-butyl-3-hexyl-1H-imidazol-3-ium (Z)-12-hydroxyoctadec-9-enoate (BHI-RA) were characterised by NMR and FT-IR.

Synthesis of Tetrabutylammonium (Z)-12-Hydroxyoctadec-9-enoate (TBA-RA)

Quantities of substrates taken: Sodium ricinoelate (1g, 0.0031 mol), TBA-Br (1g, 0.0031 mol), yield obtained 90% (1.46 g). ¹H NMR (CDCl₃, ppm): δ 5.55 (m, -CH=CH-), 5.38 (m, -CH=CH-), 3.61 (m, 1H, -CHOH), 3.31 (m, 8H, -CH₂N), 2.26 (t, 2H, -H₂CCOO), 2.18 (t, 2H, -CH₂-C=C-), 2.04 (t, 2H, -CH₂-C=C-), 1.65 (m, 8H, 4xCH₂), 1.58 (m, 2H, -CH₂), 1.43 (m, 2H, -CH₂), 1.33 (m, 12H, 6xCH₂), 1.28 (m, 12H, 6x-CH₂), 1.01 (m, 12H, 4x-CH₃), 0.88 (t, 3H, CH₃). ¹³C NMR (CDCl₃, ppm): δ 178.8, 133.2, 124.9, 71.3, 58.8, 36.6, 35.8, 31.7, 29.7, 25.5, 22.7, 19.6, 13.8. IR (CHCl₃, cm⁻¹): 3330, 3004, 2929, 2867, 1713, 1571, 1470, 1248, 749.

Synthesis of Tetrapropylammonium (Z)-12-Hydroxyoctadec-9-enoate (TPA-RA)

Quantities of substrates taken: Sodium ricinoelate (1g, 0.0031 mol), TPA-Br (1g, 0.0037 mol), yield obtained 86% (1.24 g). ¹H NMR (CDCl₃, ppm): δ 5.54 (m, -CH=CH-), 5.38 (m, -CH=CH-), 3.60 (m, 1H, -CHOH), 3.27 (m, 8H, -CH₂N), 2.20 (t, 2H, -H₂CCOO), 2.19 (t, 2H, -CH₂-C=C-), 2.02 (t, 2H, -CH₂-C=C-), 1.73 (m, 8H, 4xCH₂), 1.56 (m, 2H, -CH₂), 1.44 (m, 2H, -CH₂), 1.33 (m, 4H, 2xCH₂), 1.27 (m, 12H, 6x-CH₂), 1.03 (m, 12H, 4x-CH₃), 0.87 (t, 3H, CH₃). ¹³C NMR (CDCl₃, ppm): δ 177.3, 132.4, 125.1, 71.3, 58.6, 36.6, 31.8, 35.2, 29.6, 25.5, 22.7, 15.7, 14.1, 13.5. IR (CHCl₃, cm⁻¹): 3346, 3005, 2922, 2854, 1709, 1554, 1451, 1151, 731.

Synthesis of N,N,N-Trimethylhexadecan-1-aminium (Z)-12-Hydroxyoctadec-9-enoate (CTB-RA)

Quantities of substrates taken: Sodium ricinoelate (1g, 0.0031 mol), CTA-Br (1g, 0.0027 mol), yield obtained 88% (1.54 g). ¹H NMR (CDCl₃, ppm): δ 5.53 (m, -CH=CH-), 5.37 (m, -CH=CH-), 3.60 (m, 1H, -CHOH), 3.39 (t, 2H, -CH₂N), 3.32 (s, 9H, -CH₃), 2.48 (t, 2H, -H₂CCOO), 2.15 (m, 2H, -CH₂-C=C-), 2.02 (t, 2H, -CH₂-C=C-), 1.72 (m, 8H, 4xCH₂), 1.55 (m, 2H, -CH₂), 1.44 (m, 2H, -CH₂), 1.34 (m, 4H, 2xCH₂), 1.26 (m, 36H, 18x-CH₂), 0.88 (t, 3H, -CH₃). ¹³C NMR (CDCl₃, ppm): δ 180.4, 133.0, 125.5, 71.2, 66.9, 53.4, 37.6, 35.6, 31.8, 29.7, 25.1, 22.5, 14.1. IR (CHCl₃, cm⁻¹): 3356, 3008, 2924, 2853, 1760, 1556, 1463, 1218, 773.

Synthesis of 1-Butyl-3-hexyl-1H-Imidazol-3-ium (Z)-12-Hydroxyoctadec-9-enoate (BHI-RA)

Quantities of substrates taken: Sodium ricinoelate (1g, 0.0031 mol), BHI-Br (1g, 0.0034 mol), yield obtained 84% (1.28 g). ¹H NMR (CDCl₃, ppm): δ 7.28 (s, 1H), 7.18 (d, 2H), 5.52 (m, -CH=CH-), 5.40 (m, -CH=CH-), 5.31 (t, 2H, -CH₂N⁺), 4.34 (t, 2H, -CH₂N), 3.59 (m, 1H, -CHOH), 2.38 (t, 2H, -H₂CCOO), 2.21 (m, 4H, -CH₂-C=C-), 2.01 (m, 4H, 4x-CH₂), 1.57 (m, 2H, -CH₂), 1.40 (m, 2H, -CH₂), 1.30 (m, 4H, 2xCH₂), 1.26 (m, 18H, 9xCH₂), 1.0 (m, 8H, 4x-CH₂), 0.88 (t, 3H, CH₃). ¹³C NMR (CDCl₃, ppm): δ 180.1, 138.2, 133.1, 125.9, 121.4, 71.5, 53.4, 49.3, 37.8, 31.8, 29.9, 25.5, 22.7, 13.8, 13.4. IR (CHCl₃, cm⁻¹): 3355, 3136, 3003, 2957, 2856, 1760, 1698, 1557, 1463, 1215, 755.

Tribological Tests

Synthesized ionic liquids were analyzed for their tribological performance using four-ball tribotester (Stanhope-Seta, UK) by blending with base fluid varying concentration from 0.2 to 1.2 wt%. The anti-wear behaviour was examined as per the method ASTM D 4172 at 40 kg load and 1200 rpm for 60 min at 60-70 °C at different additive concentrations. At the end of each test, the lower three balls were washed with hexane and ether and air dried for 15 min. The scar on balls was measured with Mitutoyo toolmaker's microscope and the average of three measurements was taken as mean wear scar diameter (MWD). The load carrying capacity of ionic liquids blended base oil was analyzed as per the method IP 239 at 1475 rpm and time duration 60 sec. The analysis was carried out twice and the average of two values was reported.

Surface Characterization

Carl Zeiss (model no EVO18, Germany) scanning electron microscope (SEM) was used to study the morphology of worn surface lubricated with base oil and base oil containing ionic liquid. The elemental composition on worn surface was identified by energy dispersive X-ray spectroscopy (EDS) attached with SEM.

Thermal Properties

Differential scanning calorimeter (DSC) was used to measure the thermal properties such as melting and crystallization temperatures of synthesized ionic liquids (DSC Q-100 thermal analyzer from TA instruments). Typically, 5 ± 0.5 mg of tested sample was weighed in sealed aluminum pan and placed in the equipment chamber and maintaining continuous nitrogen flow at 50 mL/min. Both the heating and cooling cycles were performed at -100 to 100 °C at the heating rate of 5 °C/min. The melting and crystallization temperatures were determined by calculating the integrated area of concerned peaks. Thermal degradation temperature of ionic liquids was determined by thermo gravimetric analysis (TGA) using TA Q500 (TA Instruments, Inc., New Castle, DE, USA). Typically, 4-5 mg of sample was placed in α -Al₂O₃ crucible under continuous nitrogen flow of 60 mL per min at the heating rate of 10 °C/min from room temperature to 500 °C.

Results and Discussion

Synthesis and Characterization

Ricinoleic acid ((9Z, 12R)-12-hydroxy-9-octadecenoic acid) is the most abundant fatty acid in castor oil and it provides better lubricity performance due to the presence of hydroxy functionality (Drown et al., 2009; Madankar et al., 2013). Four ricinoleate anion based ILs with different types of bromine salts (TBA-Br, TPA-Br, CTB-Br and BHI-Br) were synthesized using a green synthetic route and the chemical structures of synthesized ILs is given in Fig. 1. The synthesized ricinoleate anion-based ILs were characterised by ¹H, ¹³C NMR and FTIR spectroscopy. The characteristic peak appeared at 3330-3356 cm⁻¹ in the FTIR spectrum (Fig. 2) is due to hydroxy functional group. The signals observed at 3008-3004 cm⁻¹ are due to unsaturation and the peaks appeared in the range of 1713-1698 cm⁻¹ and 1470-1451 cm⁻¹ correspond to C=O, COO stretching vibrations respectively which confirm the presence of carboxylate group. Strong vibrational bands appeared at 2929-2854 cm⁻¹ corresponding to asymmetric and symmetric C-H frequencies of the alkyl chain. The peaks present at 1470-1386 cm⁻¹ are attributed to the methylene and methyl bending modes in the cationic alkyl chains.

The peaks observed at 0.87-0.88 ppm in ¹H NMR spectra are ascribed to terminal methyl protons of fatty acid anion and the corresponding carbons in the ¹³C NMR spectra given signals at 13.4-14.1 ppm. The methylene groups in long alkyl chain of fatty acid anion exhibited proton and carbon peaks in the range of 1.26-1.73 and 15.7-31.8 ppm respectively. The methylene protons adjacent to the electronegative carboxylic group (COO-) showed downfield signals near 2.20-2.48 ppm as triplet peak. Moreover, the signals observed at 178.8-183.3 ppm and 35.8-37.8 ppm in ¹³C spectra are due to the COO- and neighbouring CH₂ carbons respectively. The unsaturated protons and the protons adjacent to unsaturation shows chemical shifts at 5.36-5.55, 2.01-2.21 ppm and their carbon signals appeared at 124.9-125.9 and 29.6-29.9 ppm respectively. The more prominent peaks appeared at 7.18-7.28 ppm and 121 ppm in ¹H and ¹³C spectra indicate the presence of aromatic protons and carbons for BHI-RA ionic liquid. The protons adjacent to the cationic centred nitrogen suffer from severe deshielding effect, these proton signals appeared at 3.27-3.39 ppm. Further moving away from the nitrogen centre the chemical shift values shifted to upfield (Gusain et al., 2016).

Thermal Properties

Thermal properties such as melting and crystallisation behaviour during the phase transition of the synthesized ionic liquids were determined by DSC thermo grams. The results obtained from the test is summarised in Fig. 3 and Table 1. Fig. 3 shows the DSC patterns of ionic liquids CTB-RA and BHI-RA. The CTB-RA exhibits the melting point at 2.6 degC during the heating cycle and crystallises at -7.8 degC during the cooling cycle. Table 1 summarises the T_m and T_c temperatures of fatty acid based IL's. It is indicating that the significant differences in their T_m and T_c were observed. The difference in their T_m and T_c might be due to the difference in their cationic structure. Imidazolium cation containing IL showed lower T_m and T_c tem-

peratures than all the quaternary ammonium salts. This is ascribed to the lower Vander Walls interaction of imidazolium cation due to sterically hindered structure. McFarlane *et al.*, stated that alkyl-imidazolium ions the geometric packing constrained the planar imidazolium ring, moreover, it has dangling alkyl chains, combined with the delocalization of the charge over the N–C–N moiety in the ring, with all of them serving to decrease the ion–ion interactions and lower the melting point (McFarlane *et al.*, 2000). The higher T_m and T_c observed for CTB-RA is due to the high Vander Walls interaction between the methylene groups, as increasing the number of methylene groups increases Vander Walls interaction which leads to higher T_m and T_c .

Thermogravimetric analysis was carried out to find the thermal decomposition stability of synthesized ILs by determining the weight loss temperature. Fig. 4 shows the thermal decomposition patterns of the ILs under the nitrogen atmosphere. Thermal stability was measured in terms of onset decomposition temperature ($T_{d(\text{onset})}$) and maximum weight loss temperature ($T_{d(\text{max})}$). The fatty acid chain length has significant effect on the thermal degradation temperature of ILs. Exclusively, the longer chain fatty acid anion containing ILs decomposed at higher temperature due to increasing Vander Waals interaction (Gusain and Khatri, 2016). All the synthesized ILs were stable up to 196 degC. On further increase in temperature these ILs gradually decomposed in the temperature range of 197-258 degC. The variation was due to difference in constituted ion structure and interactive forces (Cao and Mu, 2014; Golets *et al.*, 2016). Especially imidazolium ions provide better stability due to compact ring structure and high inter molecular interactions (Maton *et al.*, 2013). All the four ILs exhibited high thermal stability hence, these synthesized ILs are effective lubricant additives for base oil operating at high temperature.

Antiwear Performance

A series of wear tests was conducted to evaluate the antiwear behaviour of synthesized ILs in two different base oils EKE and DOS by varying the concentration (wt %) of additives. Fig. 5 (a and b) illustrates the variation in wear scar diameter (WSD) with IL concentration. There observed decrease in WSD by increasing the concentration from 0.2 to 0.8 wt%. At 0.8 wt% all the four synthesized ILs showed excellent antiwear performance in two base oils. Further increasing the additive concentration to 1.0 and 1.2 wt% no significant reduction in WSD was observed thus 0.8 wt% was taken as optimized additive concentration. Higher wear scar above the optimized concentration might be due to the adsorption of excess amount of additive on the metal surface, which leads to coagulation and causes severe damage to the tribofilm by increase in frictional force and results in excess wear on rubbing surface (Wang *et al.*, 2013). Fig. 5 illustrates that all the synthesized ILs showed lower WSD in both base oils at all the concentrations. Exclusively, the additive BHI-RA exhibited maximum reduction in WSD of both base oils. WSD of base oil EKE reduced from 0.846 to 0.602 mm and in the case of DOS it is from 0.872 to 0.617 mm. The presence of TBA-RA, TPA-RA, CTB-RA and BHI-RA in base oil EKE significantly reduced the WSD by 17, 21, 25 and 28 % respectively whereas, 38% reduction in WSD was observed with commercially available antiwear additive Lubrizol 1359. Overall, the order of antiwear behavior is as follows: BHI-RA > TBA-RA > TPA-RA > CTB-RA. Remarkable variation in antiwear behaviour among the four ILs indicates that the WSD is dependent on composition of IL. The antiwear behaviour of BHI-RA is slightly better than others which could be ascribed to the presence of heterocyclic imidazole ring. Variation in antiwear performance of TBA-RA and TPA-RA could be attributed to the alkyl chain length difference on quaternary ammonium ion. According to Gusain *et al.* (2017), longer alkyl chain containing quaternary ammonium ILs provide better lubrication performance than the shorter chains. Thus the IL TBA-RA showed better antiwear performance compared to TPA-RA.

The effect of applied load on WSD was also studied in order to estimate the performance of synthesized ILs at higher loads. The tests were conducted by varying the loads from 40 to 80 kg at optimized IL concentration (0.8 wt%) and rotation speed (1200 rpm) at 60 minutes run time and the results were presented in Fig. 6. It clearly illustrates that at the initial load (40 kg) WSD of the two base oils is very high whereas, IL blended base oil exhibited lower WSD. Further increase in the load from 40 to 80 kg resulted increase in WSD but this increase is comparatively minimum to the neat base oil. This is may be due to decrease in the thickness of tribofilm between rubbing surfaces with increasing load (Yan *et al.*, 2014).

WSD as a function of the rotation speed was also studied at optimized additive concentration (0.8 wt%) and load 40 kg at 60 minutes run time by varying the rotation speed from 1200 to 1742 rpm and the results were presented in Fig. 7. The minimum WSD was observed with base oil and base oil blended additive at 1200 rpm meanwhile, raising the rotation speed from 1200 rpm to 1742 rpm increase in WSD was observed. This is due to break out of tribofilm caused by increasing entrainment force (Hu et al., 2013). Above experimental results indicate that the synthesized ILs are good tribo active additives to reduce the WSD of tested base oils even at higher load and rotation speed.

Extreme Pressure Performance

The extreme pressure (EP) behaviour of the synthesized ILs was analyzed in two base oils and the results were shown in Fig. 8. It can be seen that the weld point of two base oils improved with addition of synthesized ILs. The base oils EKE and DOS exhibited weld points 160 and 120 kg respectively, further the addition of ILs showed significant enhancement in weld points due to the development of effective tribofilm on the rubbing surface. Fig. 8 compares the weld points of base oils with different IL concentration from 0.25 wt% to 1.5 wt%. While increasing the concentration from 0.25 to 1.25 wt% increase in weld point of the base oil was observed and further increasing the concentration to 1.5 wt% resulted in decrease of weld point, thus 1.25 wt% is taken as the optimized additive concentration. At this particular concentration all the synthesized additives were greatly effective in improving the weld point of the two base oils. The IL's BHI-RA, TBA-RA, TPA-RA and CTB-RA enhanced the weld point by 43, 31, 25 and 25% respectively in base oil EKE. Exclusively, BHI-RA exhibited superior extreme pressure performance in both base oils. Yang et al. reported that the nitrogen containing heterocyclic compounds are capable to develop strong tribofilms under extreme pressure conditions (Yang et al., 2013). The weld points obtained with all the synthesized ILs were compared with commercially available additive dibenzyl disulfide (DBDS) and the results indicate that the synthesized ILs exhibited either comparable or better EP performance to DBDS.

Surface Morphology

SEM analysis was carried to study the surface morphology of steel balls after the wear tests. Fig. 9 (a and b) and Fig. 10 (a and b) shows the morphology of worn surface of steel balls lubricated by base oil EKE and EKE containing IL (BHI-RA), base oil DOS and DOS containing IL (BHI-RA) respectively. It can be observed that the base oil lubricated surface is quite rough with wide scratches and deep furrowed wear tracks which are signs of mordant wear. Whereas, the surface lubricated with base oil containing IL is smoother with few scratches and wear tracks which is in well accordance to the efficient antiwear behaviour of IL. These results show that a stable tribofilm formed with additive to prevent the direct contact between interacting surfaces (Ing et al., 2012). Fig. 11 (a and b) shows the EDX spectrum of worn surface lubricated with base oil EKE, DOS and base oil blended with BHI-RA (Fig. 11 (c and d)). It can be seen that the surface lubricated by neat base oil EKE and DOS shows iron, carbon and oxygen signals whereas, surface lubricated with IL blended base oil showed additional nitrogen signal. These findings further suggest that the incorporation of nitrogen on the surface provide the protection against severe wear damage.

Conclusion

Four novel ricinoleate anion-based ionic liquids were synthesized by metathesis of sodium ricinoleate with bromide salts and were evaluated as green lubricant additives in two base oils EKE and DOS. The synthesized additives exhibited excellent thermal stability and tribological performance. At optimal IL concentration the fatty acid constituted ILs greatly reduced the wear scar diameter and improved the weld point of both base oils. The results obtained from tribological tests confirmed that there is a significant effect of changing the cation on their tribological performance. The ionic liquids BHI-RA and TBA-RA exhibited better tribological performance compared to TPA-RA and CTB-RA under boundary lubrication conditions. Elemental mapping and worn surface morphology studies further confirmed the deposition of tribofilm by ricinoleate constituted ionic liquid. This study illustrates that fatty acid constituted ILs are excellent lubricating oil additives to minimize or replace the use of environmentally hazardous ILs.

Supplementary Information (SI)

This includes data for ^1H , ^{13}C NMR and FTIR spectra of synthesized ionic liquids

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Figure Captions

Fig. 1 Chemical structures of synthesized ionic liquids

Fig. 2 FT-IR spectra of synthesized ionic liquids

Fig. 3 Differential scanning calorimetric thermo grams of (a) CTB-RA and (b) BHI-RA

Fig. 4 TGA curves of ionic liquids under nitrogen atmosphere

Fig. 5 Variation of wear scar diameter with different concentrations of additives in base oil (a) EKE and (b) DOS

Fig. 6 Variation of wear scar diameter with different loads of additives in base oil (a) EKE and (b) DOS

Fig. 7 Variation of wear scar diameter with different rotation speed (rpm) of additives in base oil (a) EKE and (b) DOS

Fig. 8 Weld points at different concentration of additives in base oil EKE and DOS

Fig. 9 SEM images of the worn surface lubricated with (a) EKE and (b) EKE containing 0.8% of BHI-RA

Fig. 10 SEM images of the worn surface lubricated with (a) DOS and (b) DOS containing 0.8% of BHI-RA

Fig. 11 EDS analysis of the worn surfaces lubricated with (a) EKE, (b) DOS, (c) EKE containing 0.8% of BHI-RA and (d) DOS containing 0.8% of BHI-RA

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